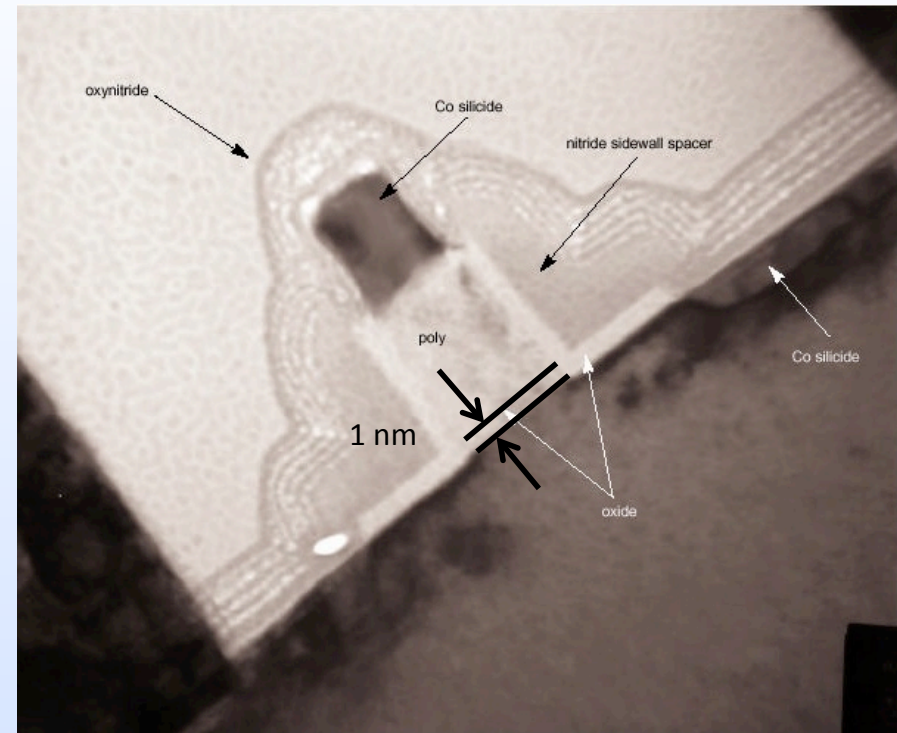
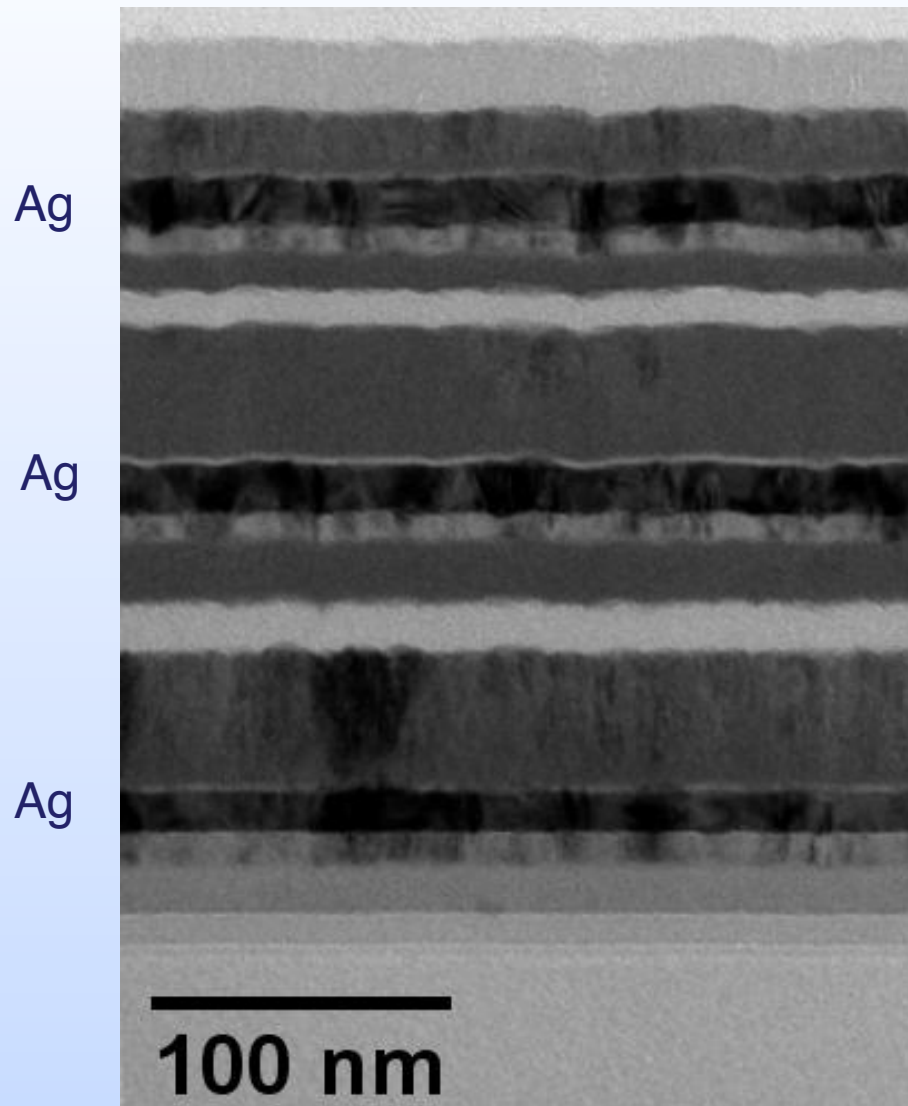


# Thin Film Deposition

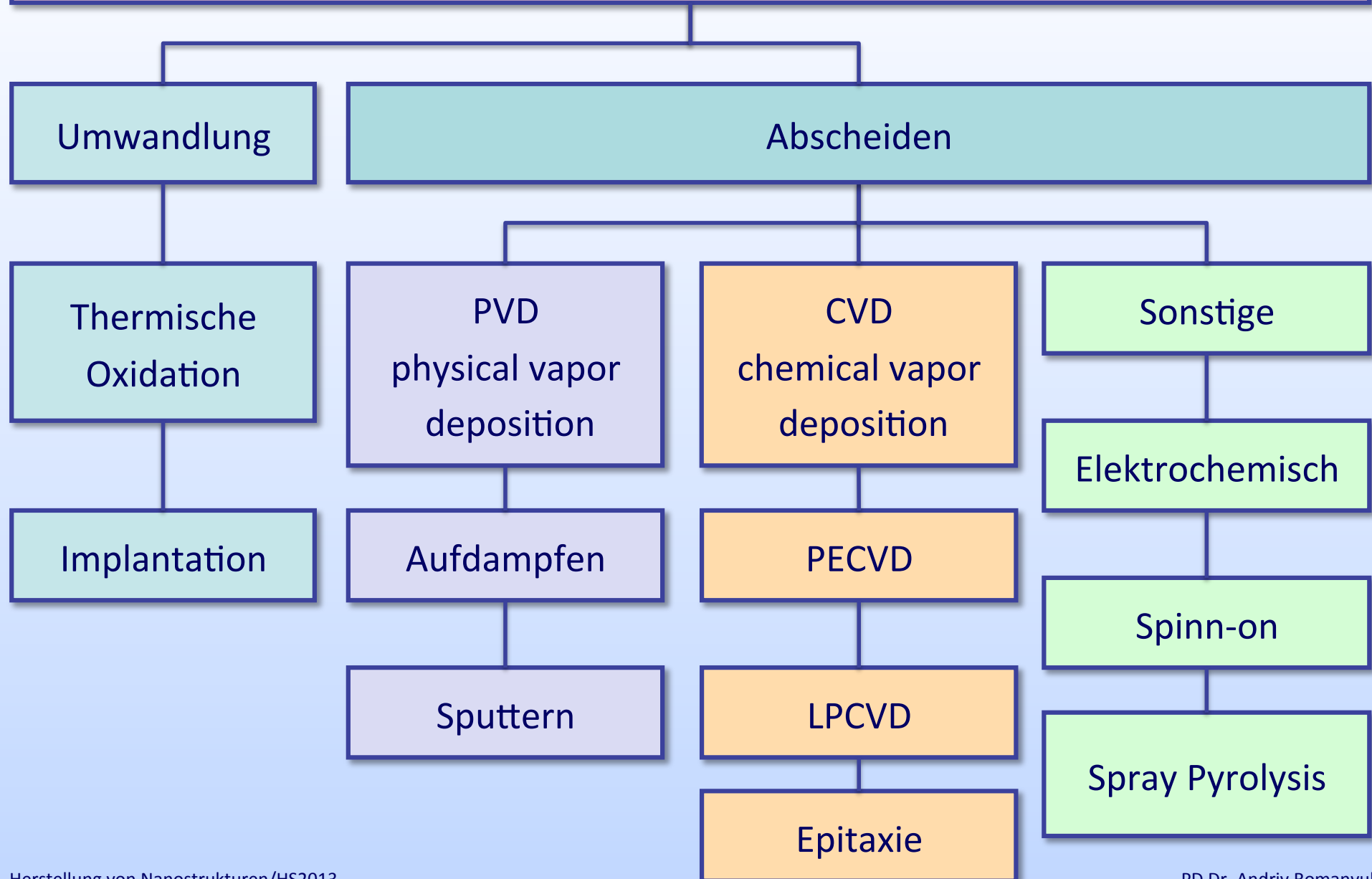
## Wann spricht man von „dünnen Schichten“



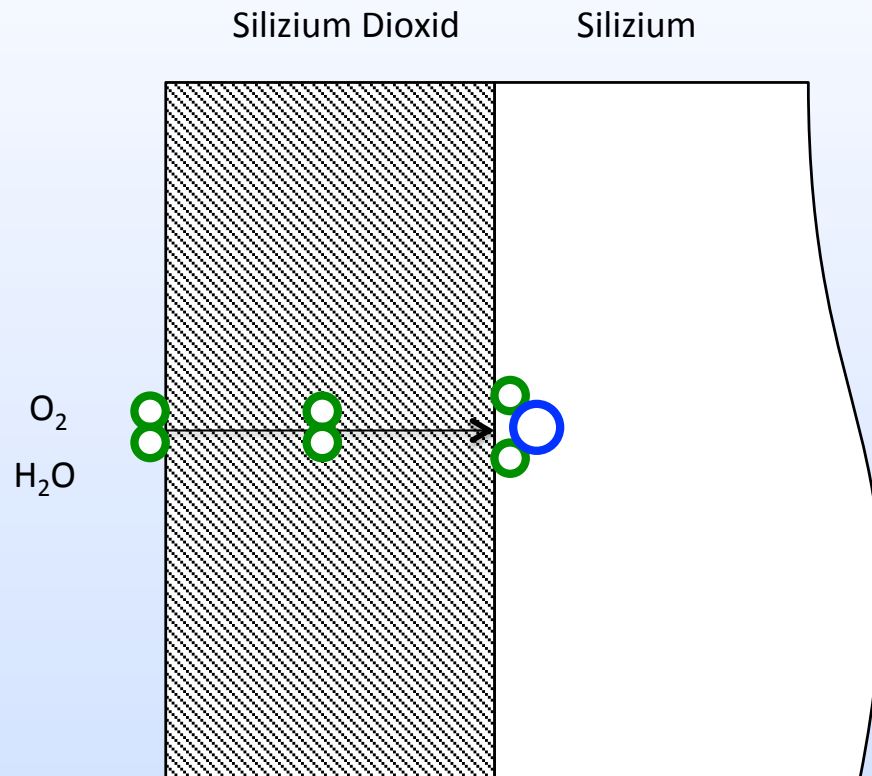
### Typische Schichtdicken ...

- von wenigen atomaren Lagen
- bis zu circa 20  $\mu\text{m}$

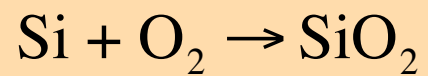
# Erzeugung dünner Schichten



# Thermische Oxidation

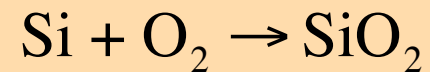


1. Diffusion des Sauerstoffes/  
Wassers bis zur Oxidoberfläche
2. Diffusion des Sauerstoffes/  
Wassers durch das bereits  
gebildete Oxid bis zur  
Grenzschicht
3. Chemische Reaktion an der  
Grenzschicht



# Thermische Oxidation

## 1. Prozessvariante: **trockene Oxidation** mit Sauerstoff

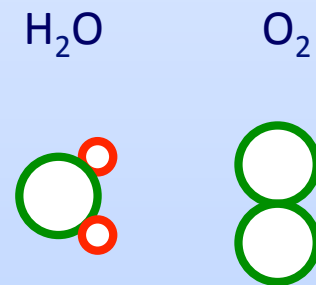


- T = 800°C – 1200°C
- sehr gute Qualität des Oxides
- geringe Aufwachstraten

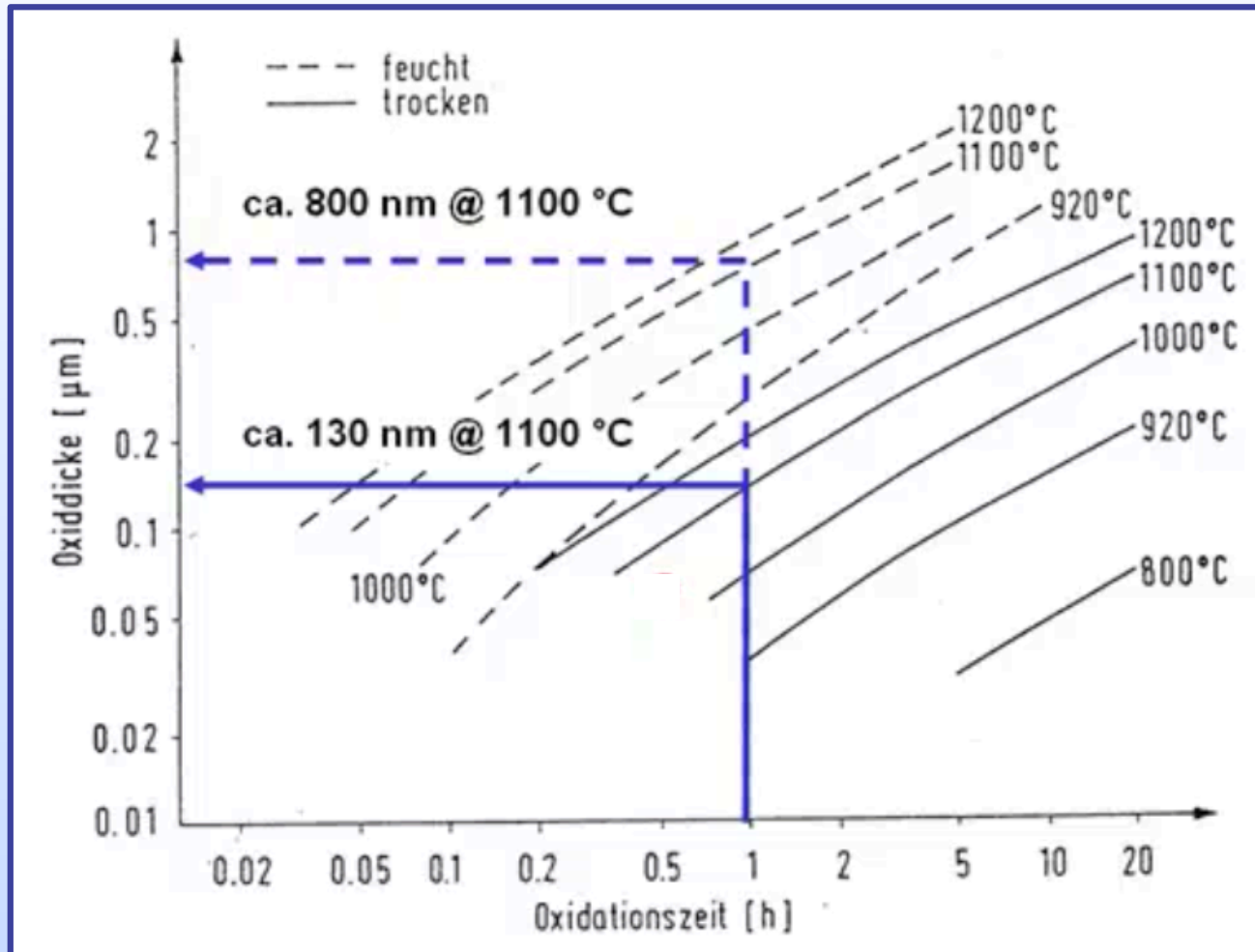
## 2. Prozessvariante: **nasse Oxidation** mit Wasserdampf



- T = 900°C – 1100°C
- höhere Reaktionsrate
- Verunreinigung des Oxides mit Wasser



# Thermische Oxidation



- Diffusionskonstante

$$D = D(p, T)$$

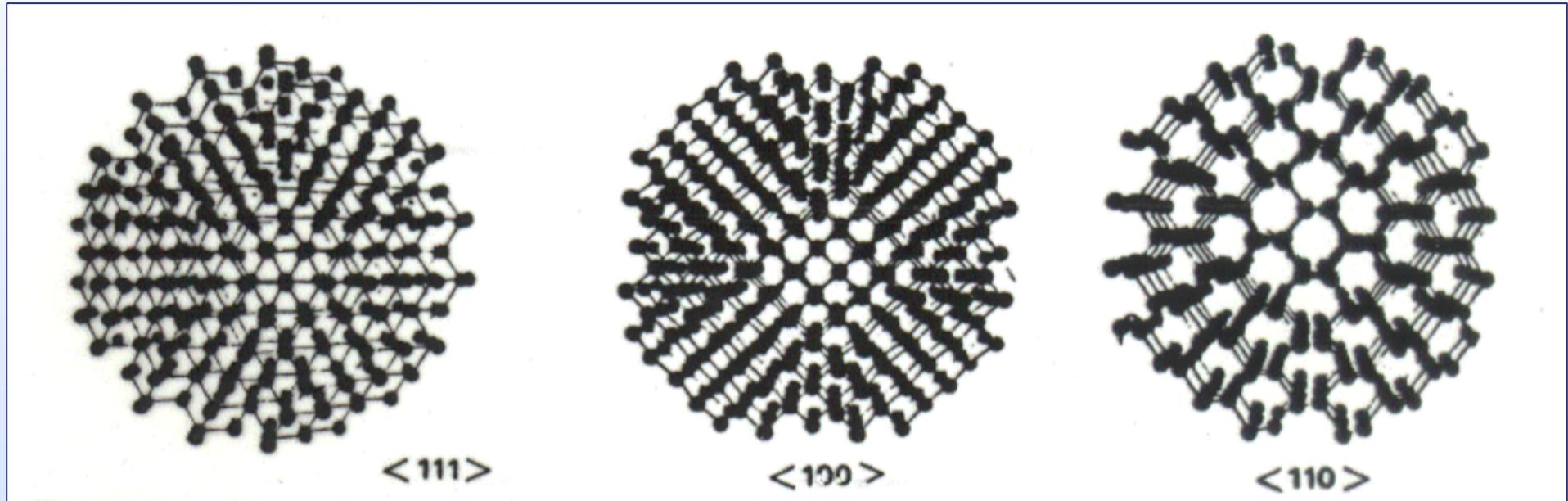
- Diffusionslänge

$$L = \sqrt{D\tau}$$

- Diffusionszeit

$$\tau = \frac{L^2}{D}$$

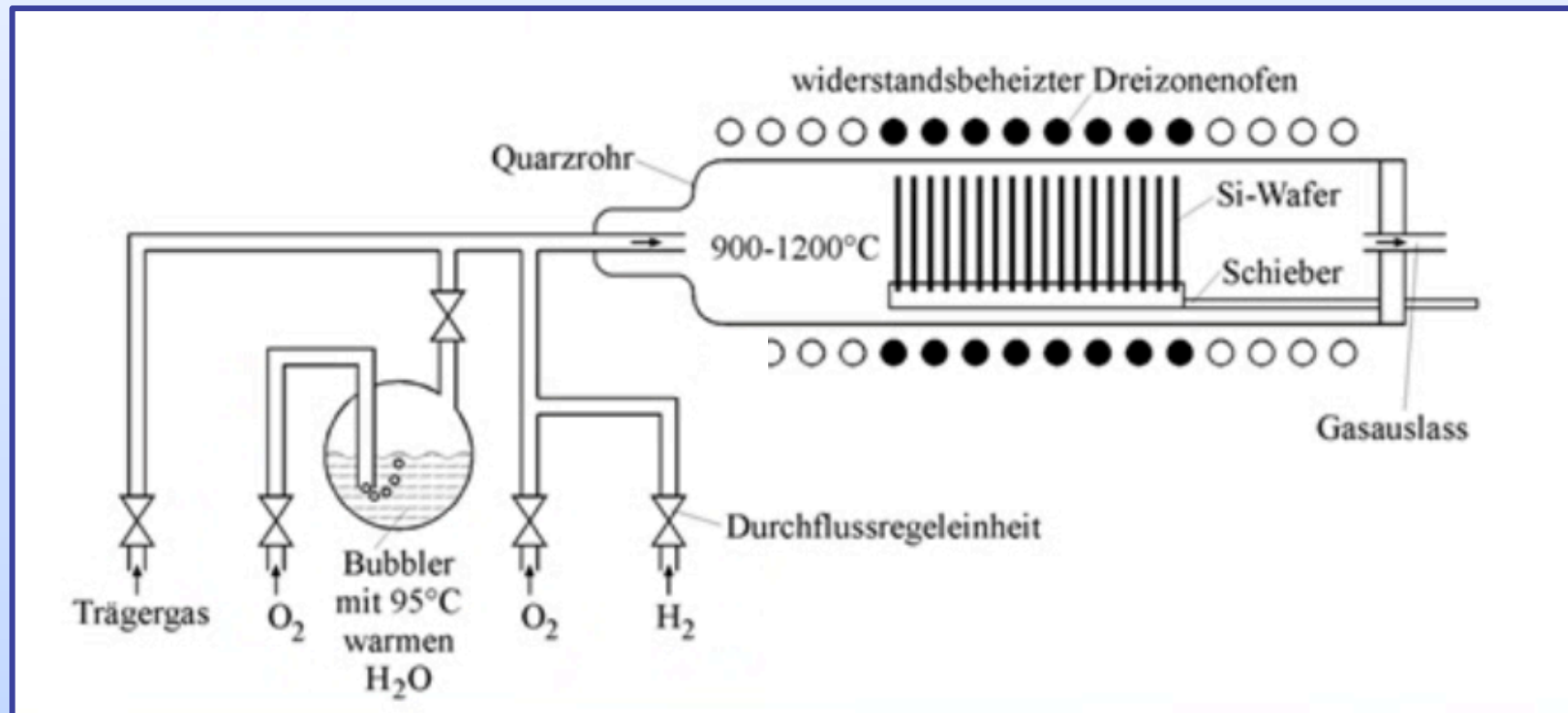
# Thermische Oxidation



- Wachstumsrate ist auch abhängig von der Kristallorientierung
- (111) Silizium oxidiert 1.7 mal so schnell wie (100) Silizium
- Für die Diffusion ist die  $\text{SiO}_2$  Schicht und nicht Si-Kristall relevant

# Oxidationsofen

- Meist widerstandsbeheizte Dreizonenofen
- Gasregleinheit und Bubbler
- Temperaturprofil mit  $\pm 0.5^\circ\text{C}$  über eine Länge von einem Meter

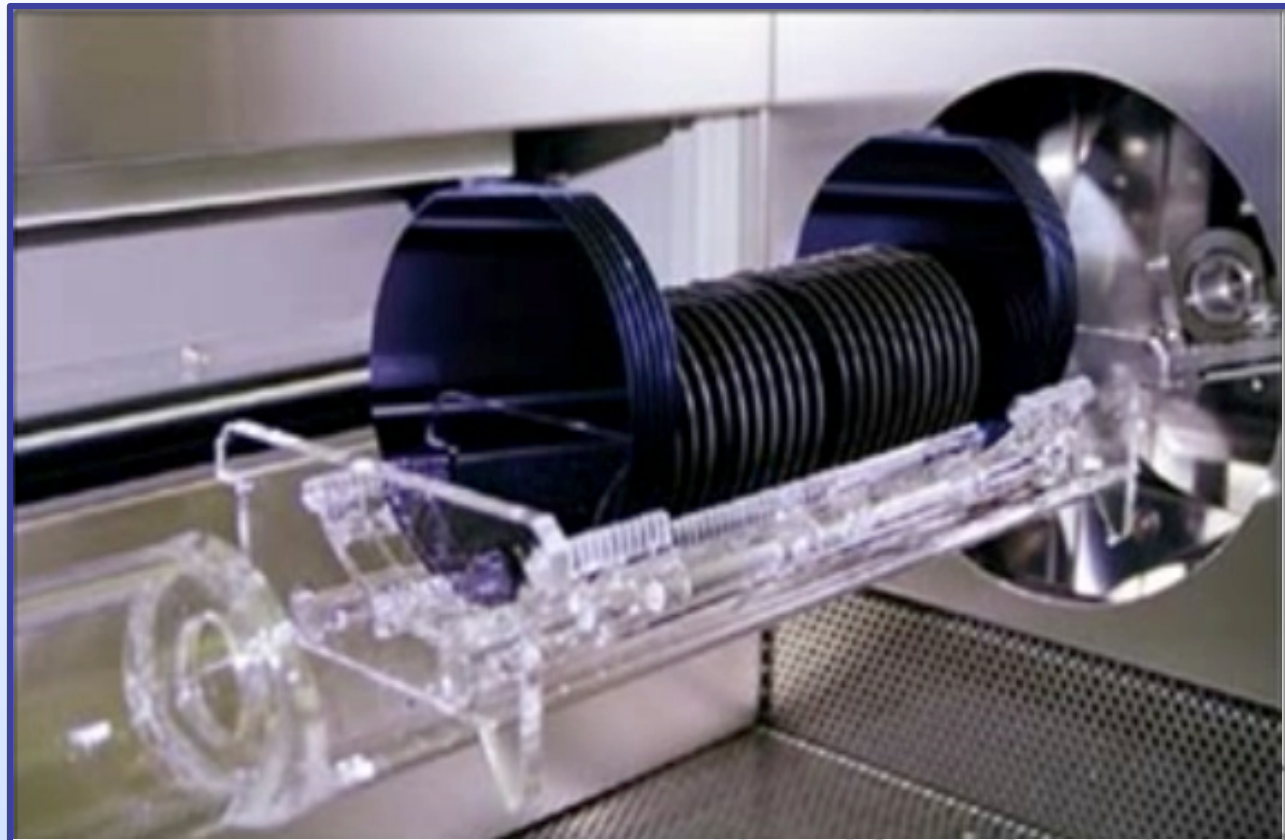




## Beispiel für einen Oxidationsofen

### Prozesse:

- Oxidieren
- Tempern
- Dotieren
- LPCVD

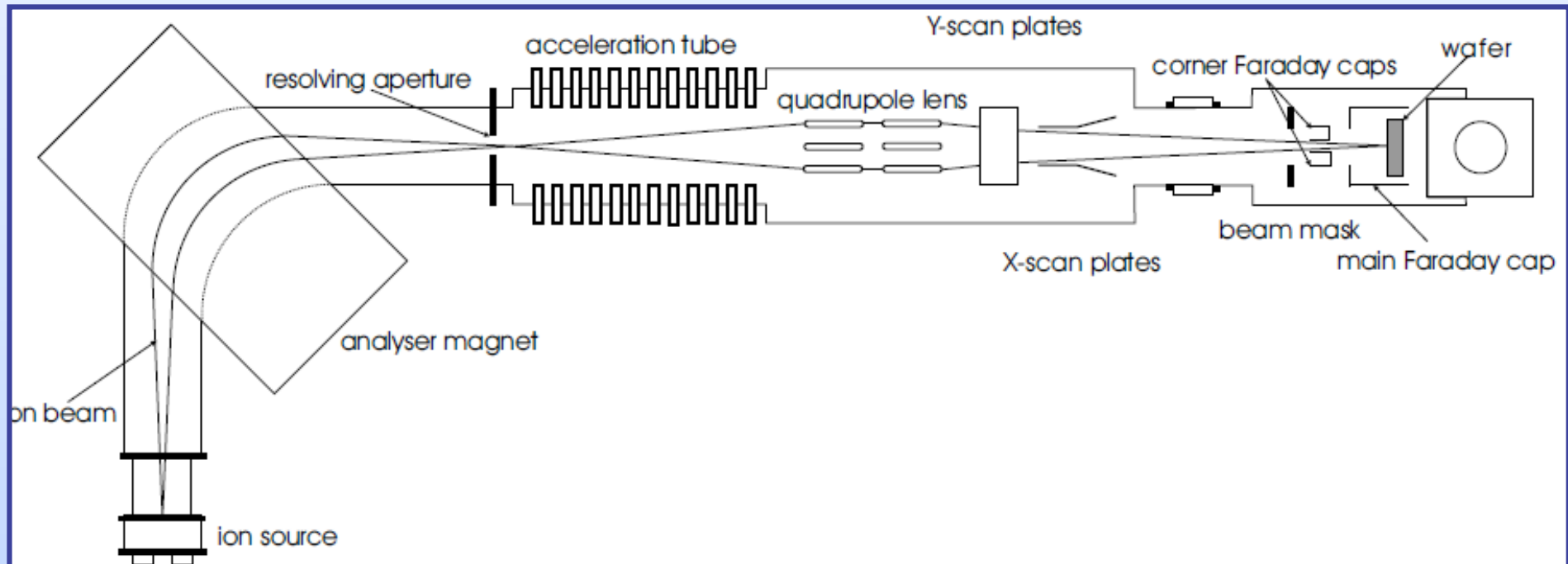


- Typische Batch-Grösse: 50 Wafers
- Hohe Anforderungen an Reinheit aufgrund hoher Temperaturen

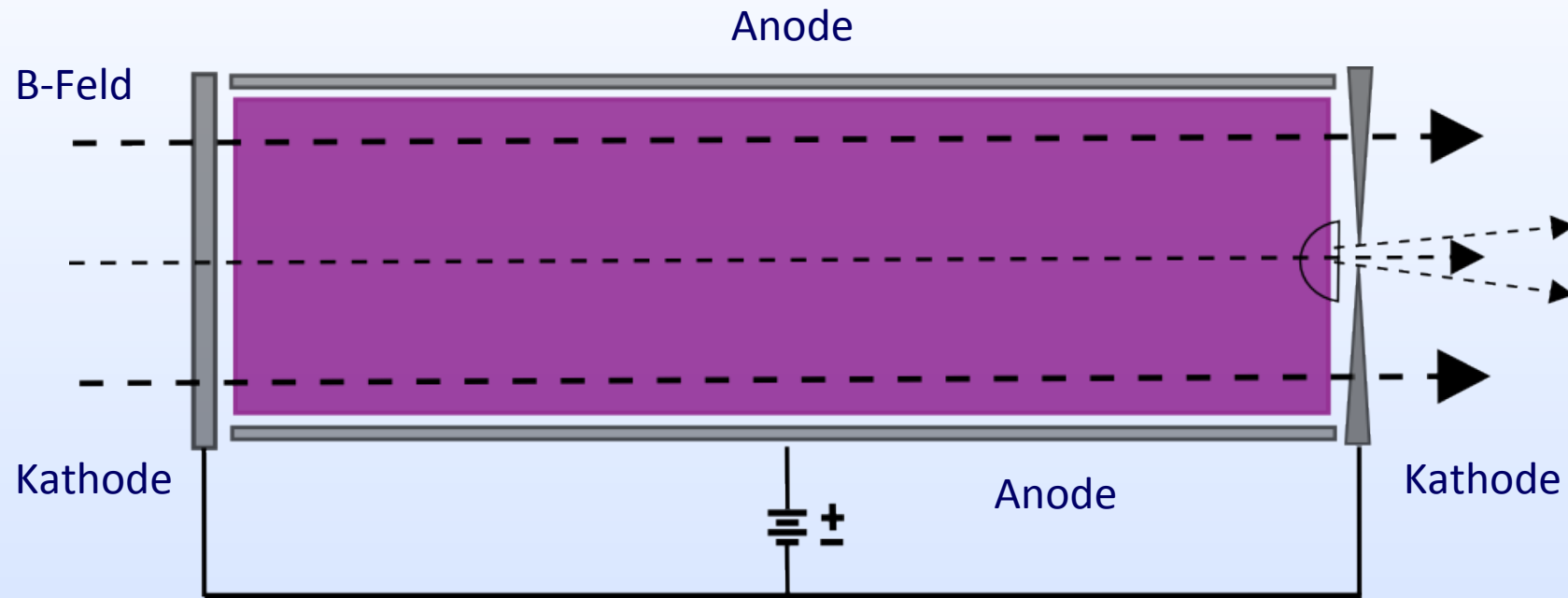
# Ionenimplantation

# Ionenimplantation

1. Ionisierung, Extraktion
2. Mass-Separation
3. Beschleunigen



# Penning Ionenquelle



## Typische Betriebsparameter:

$$P_{Ar} = 1 \text{ Torr}$$

$$V = 500 \text{ V}$$

$$I = 1.5 \text{ A}$$

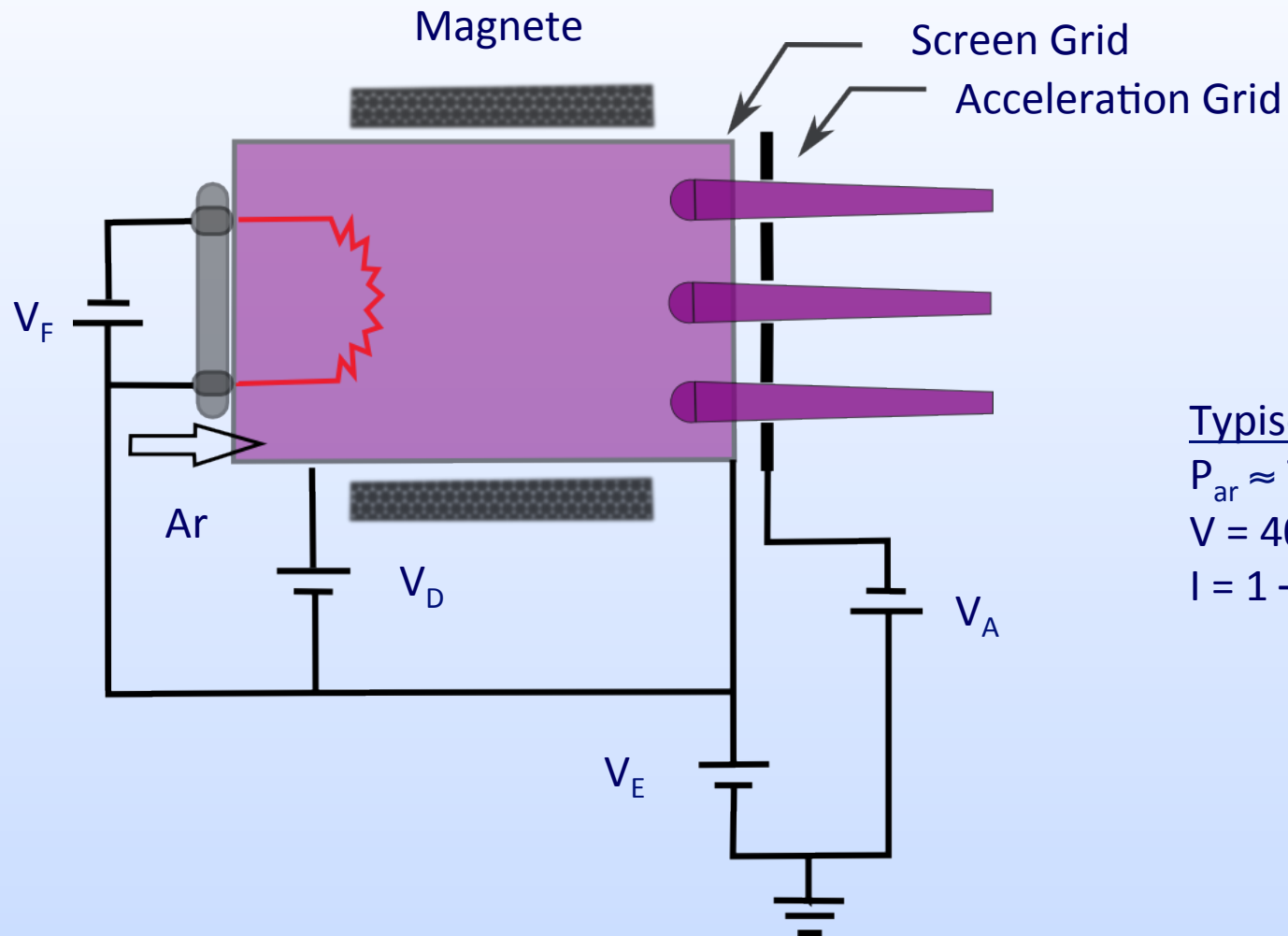
## Vorteile:

- einfach
- billig

## Nachteile:

- Strom und Spannung sind abhängig
- keine Fokussierung
- Kontaminationen

# Kaufman Ionenquelle



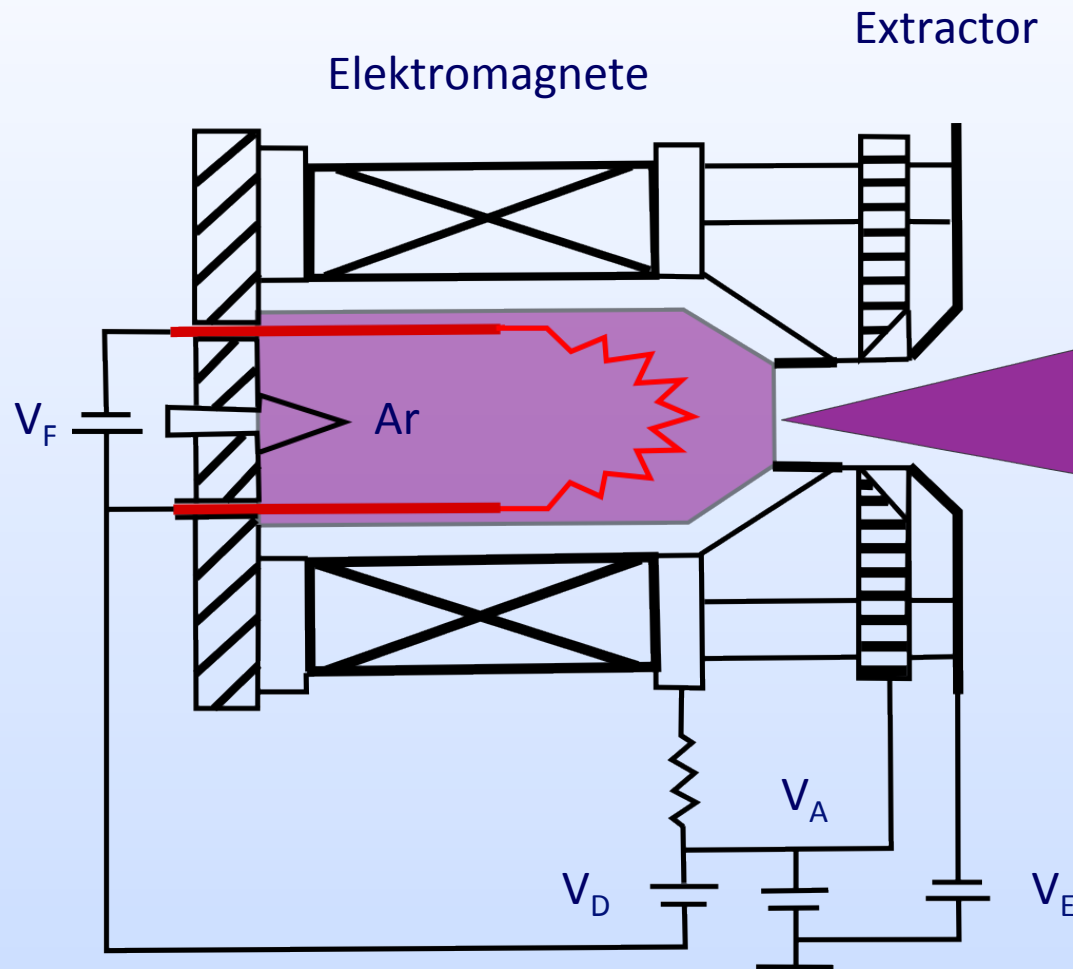
Typische Betriebsparameter:

$$P_{\text{ar}} \approx 7 \text{ mTorr}$$

$$V = 40 \text{ V}$$

$$I = 1 - 2 \text{ A}$$

# Duoplasmatron



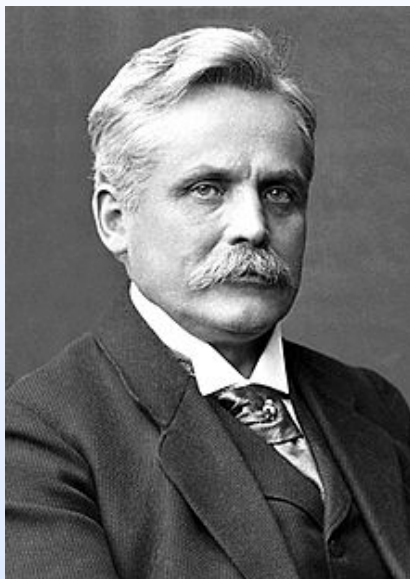
Typische Betriebsparameter:

$$P_{\text{Ar}} = 7 - 100 \text{ mTorr}$$

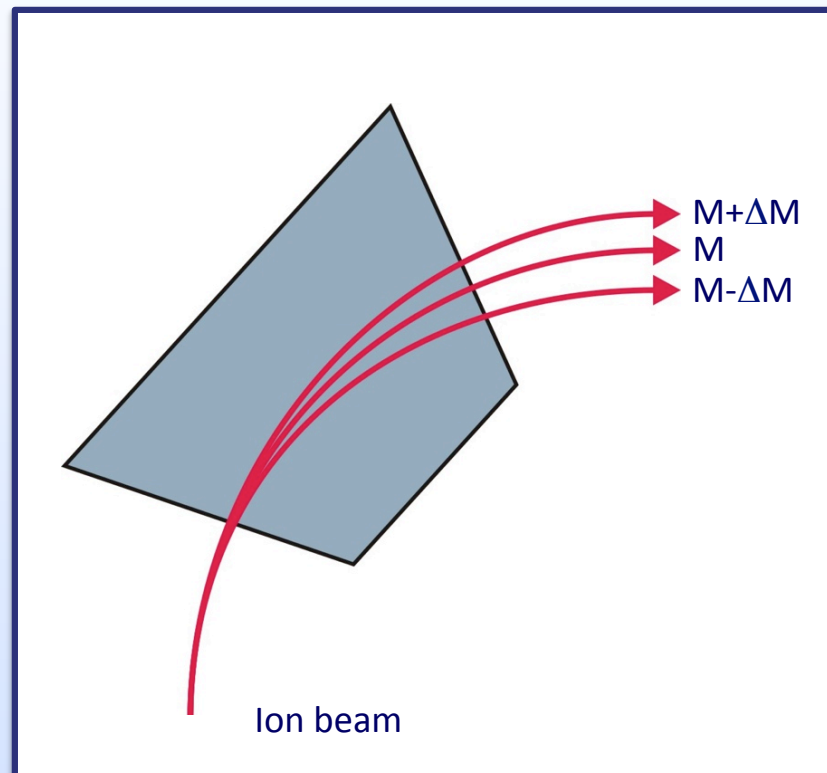
$$V = 80 \text{ V}$$

$$I = 1 - 2 \text{ A}$$

# Sektor Mass Spectrometer



Wilhelm Carl Werner  
Otto Fritz Franz Wien  
(1864 – 1928)



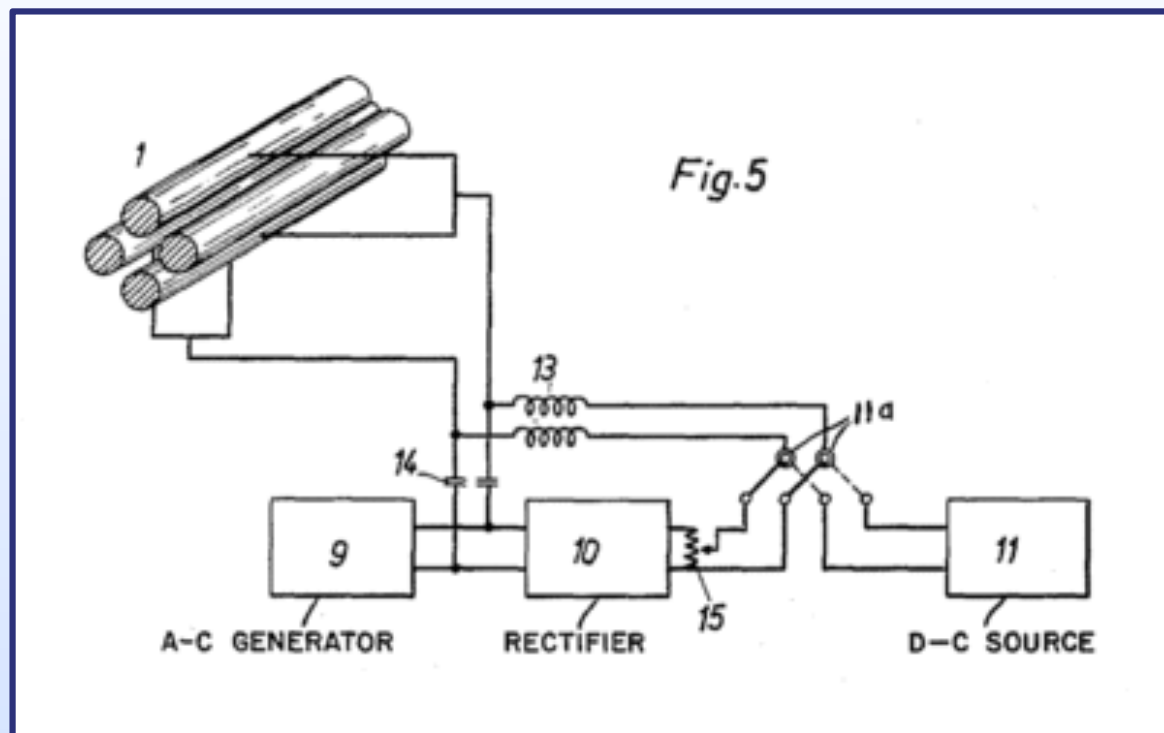
- High mass resolution
- High transmission
- Slow peak switching

$$\frac{m}{e} = \frac{B^2 r^2}{2V} \text{ mit } V = \sqrt{\frac{2eU}{m}}$$

# Quadrupole Mass Spectrometer



Wolfgang Paul  
(1913 – 1993)

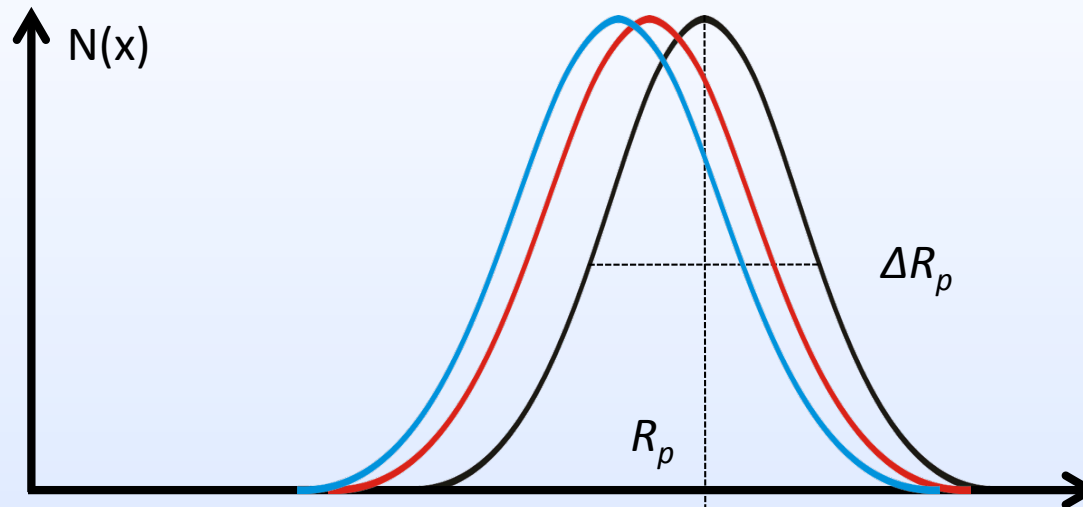


"Apparatus For Separating Charged Particles Of Different Specific Charges" Patent number: 2939952

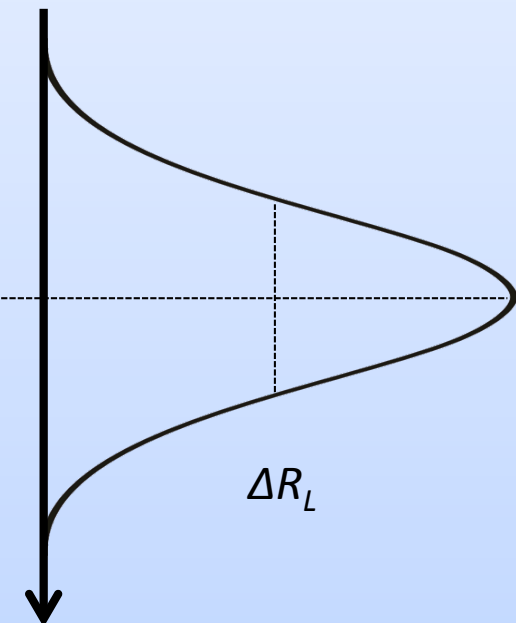
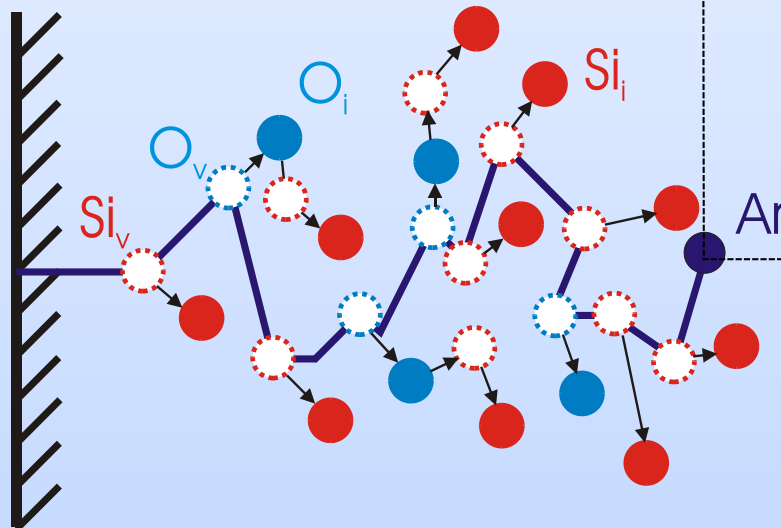
- Fast peak switching
- Low mass resolution
- Low transmission



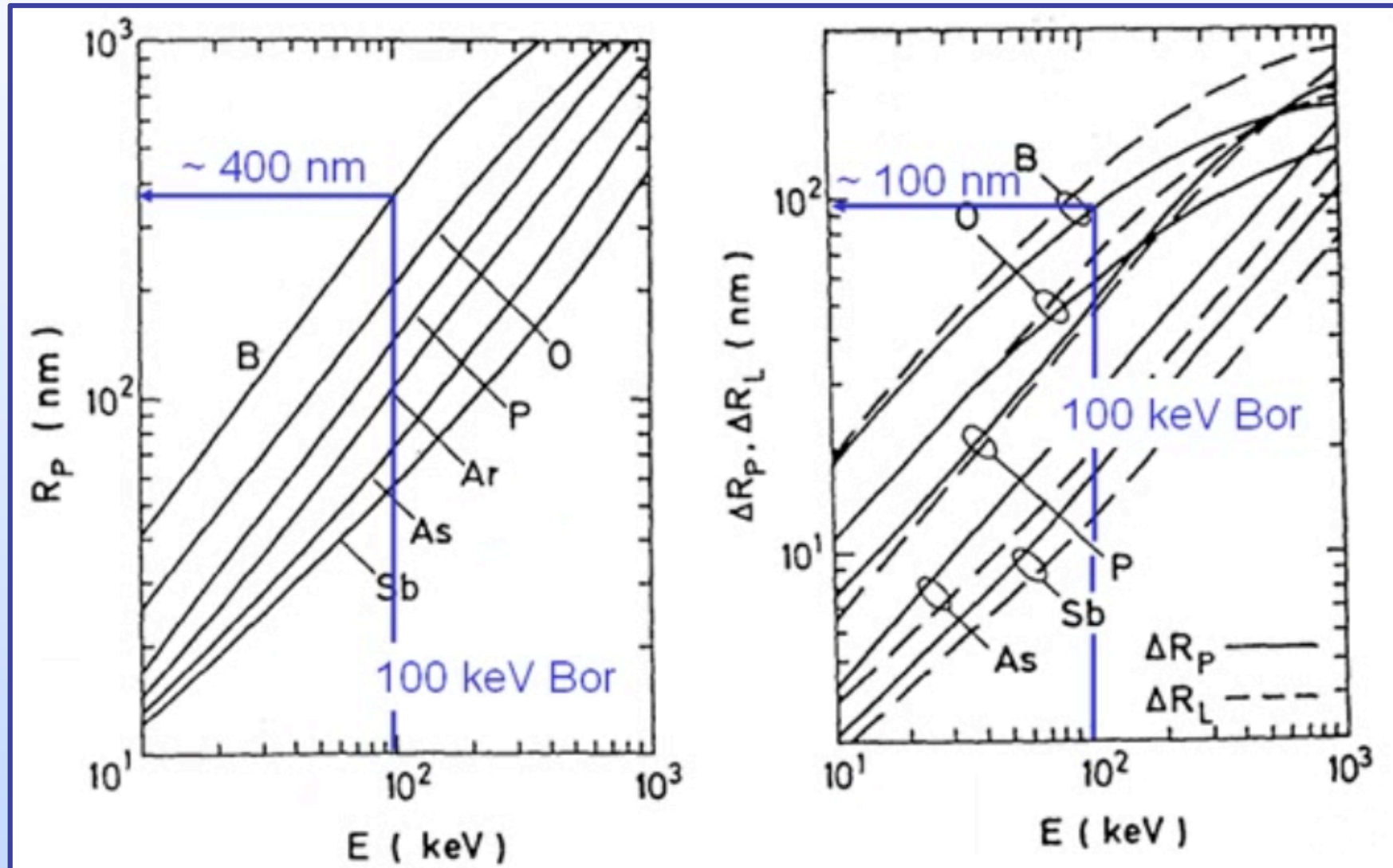
# Collision Cascade



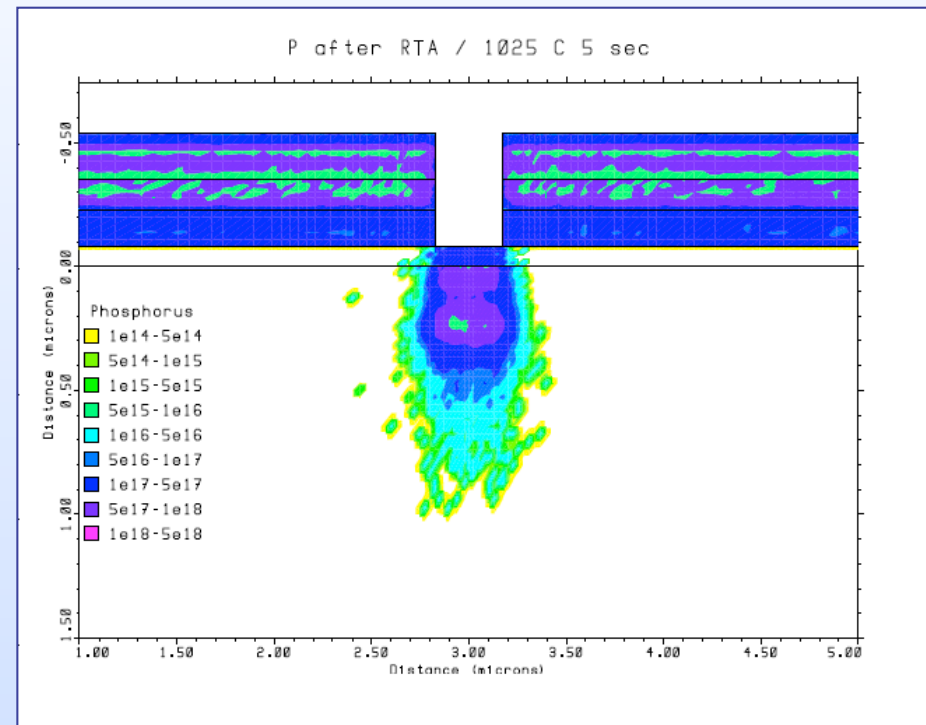
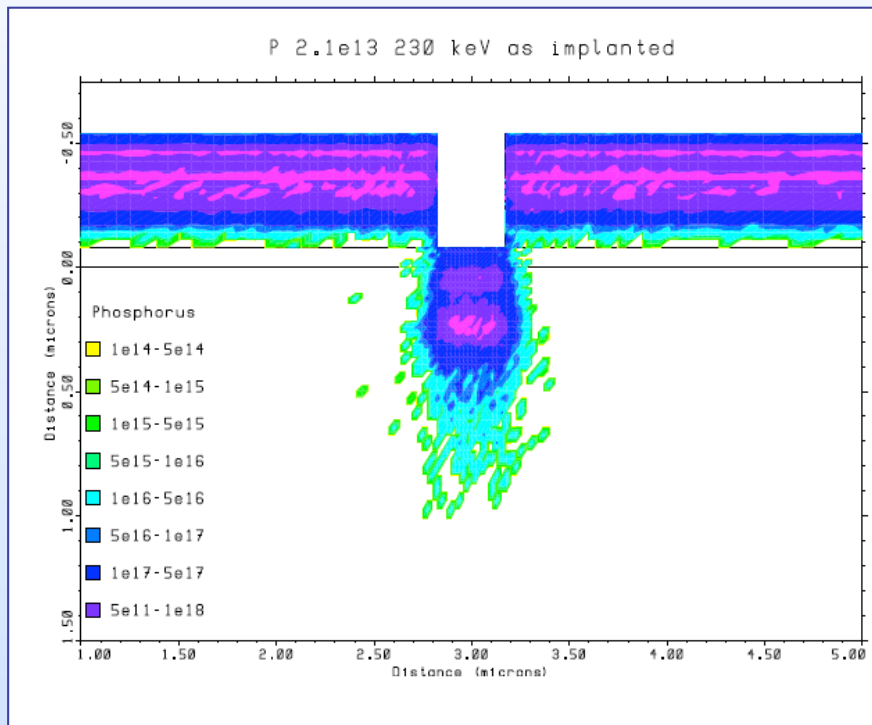
- Streuprozesse werden statistisch behandelt (Mittelung)
- Dotierprofil ist näherungsweise gaussförmig



# Reichweite, Streubreite & laterale Abweichung

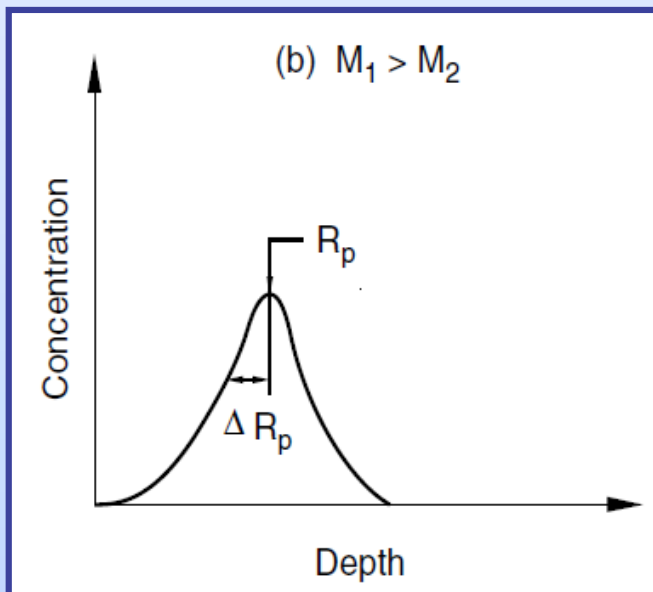
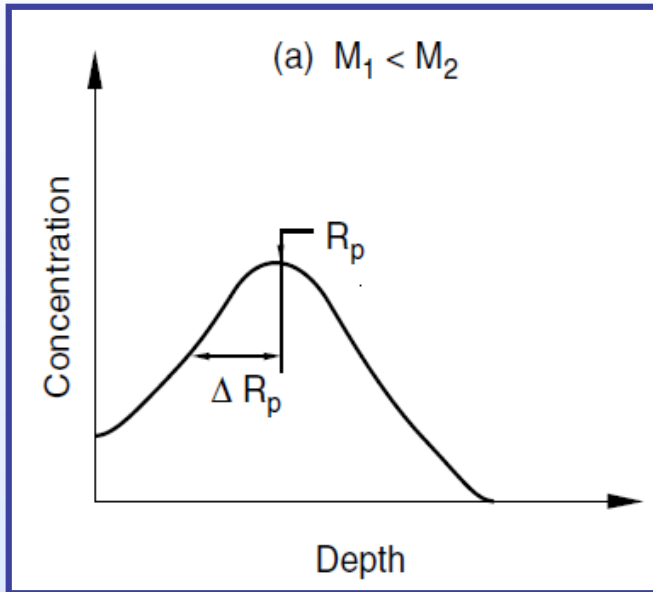


# p-Well implantation



- **SRIM** (Stopping and Range of Ions in Matter): Monte Carlo simulation of transport properties of ions in matter
- **TSUPREM, TAURUS**: Monte Carlo simulation & diffusion processes

# Profile parameters



Dose

$$\phi = \int_0^{\infty} C(x) dx$$

Projected Range

$$R_P = \frac{1}{\phi} \int_0^{\infty} x \cdot C(x) dx$$

Longitudinal Straggle

$$(\Delta R_P)^2 = \frac{1}{\phi} \int_0^{\infty} (x - R_P)^2 \cdot C(x) dx$$

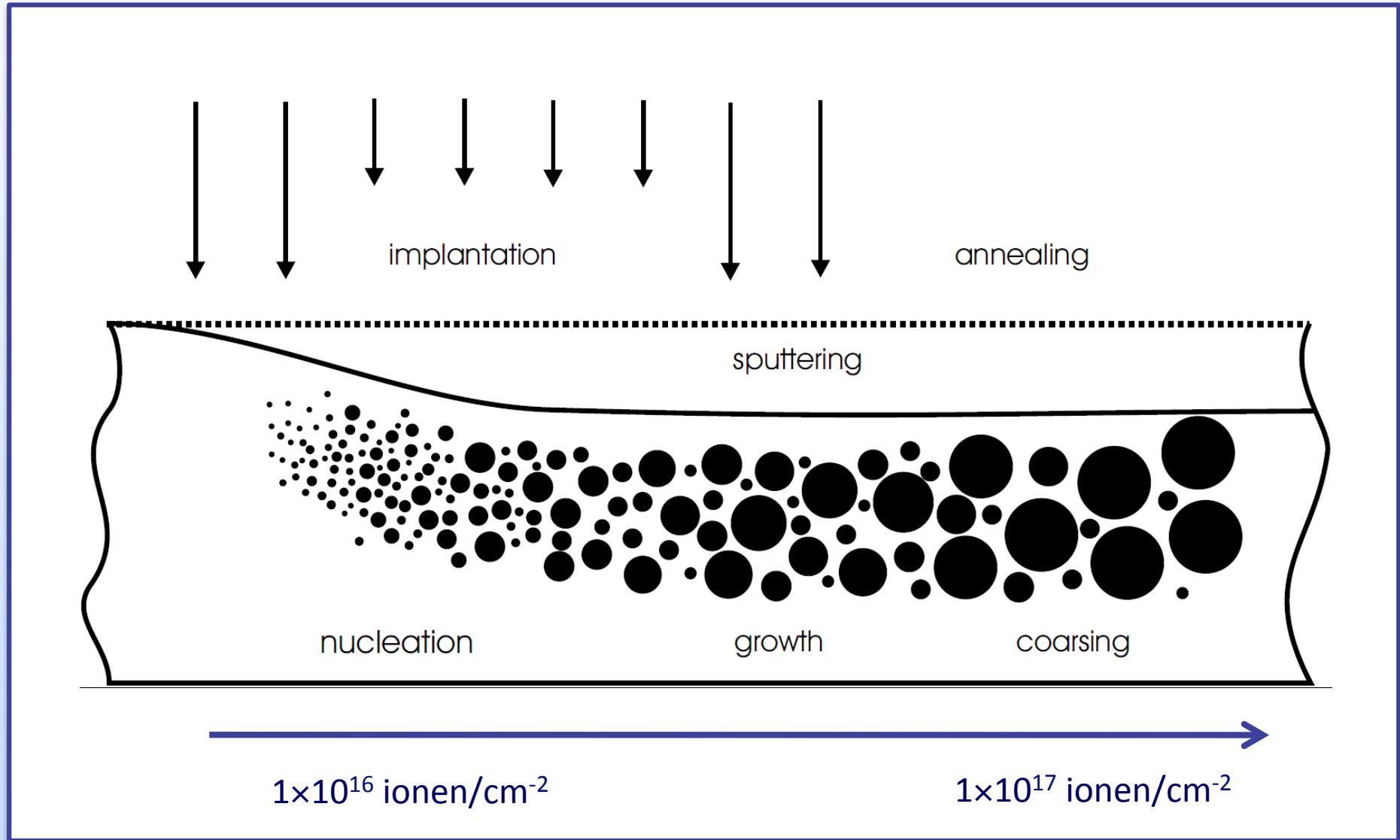
Skewness

$$\propto \frac{1}{\phi} \int_0^{\infty} (x - R_P)^3 \cdot C(x) dx$$

Kurtosis

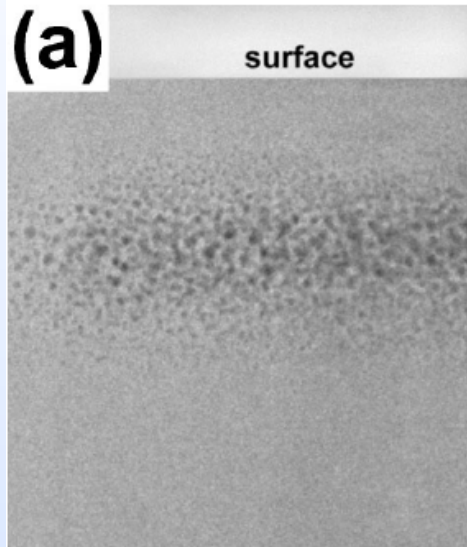
$$\propto \int_0^{\infty} (x - R_P)^4 \cdot C(x) dx$$

# Ion implantation: Dose dependency

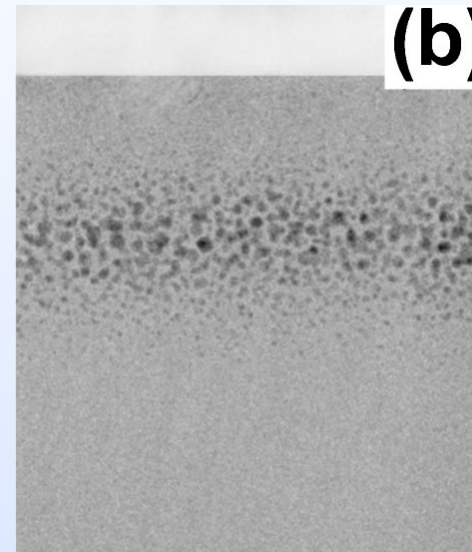


# Nanoparticle formation

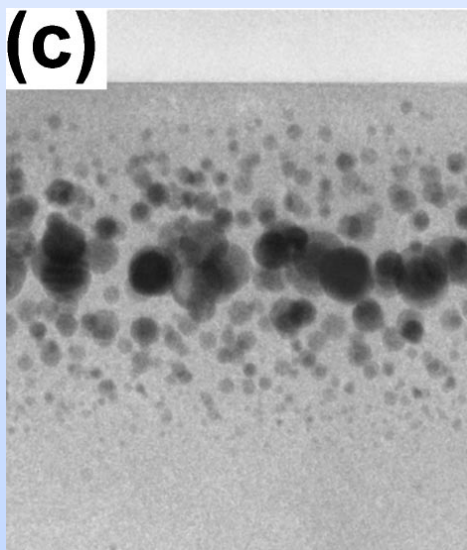
Implantation:  $3 \times 10^{16} \text{ cm}^{-2} \text{ Au}^+$  into  $\text{SiO}_2$  @  $E = 190 \text{ keV}$



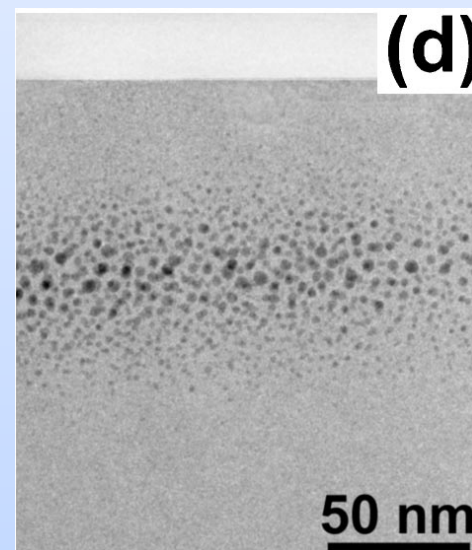
1h 400°C in air



1h 700°C in air



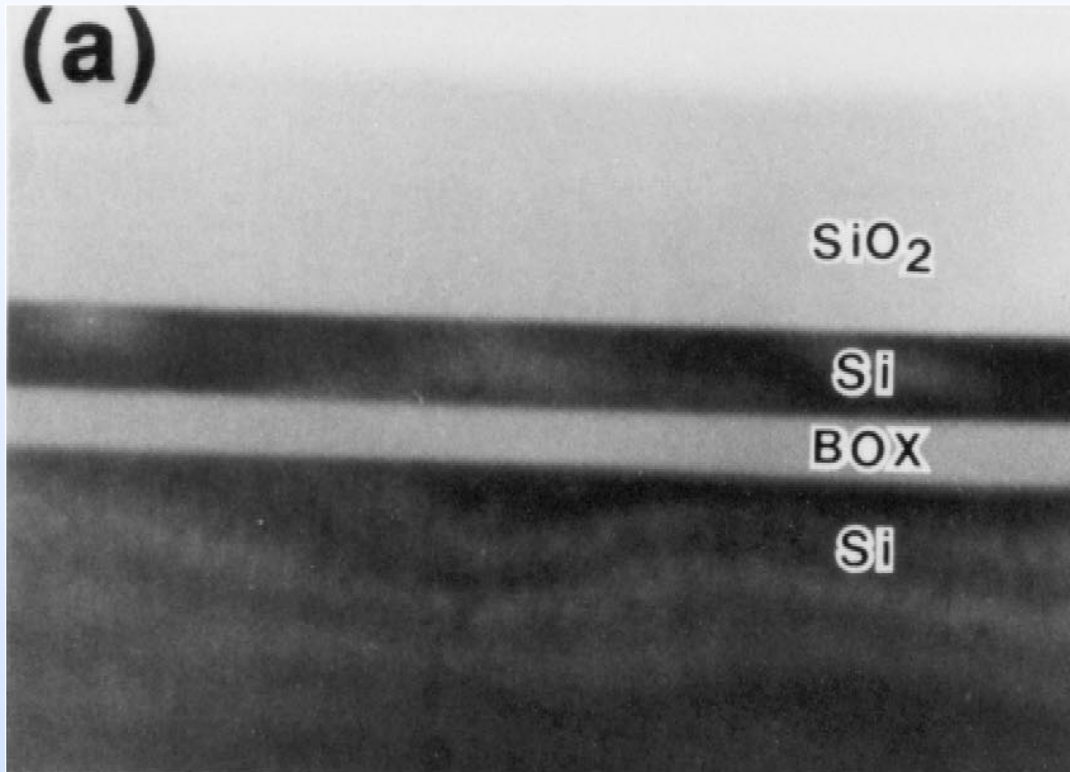
1h 900°C in air



1h 900°C in Ar

50 nm

# Separation by Implanted Oxygen (SIMOX)



Implantation:

$2 \times 10^{17} \text{ cm}^{-2} \text{ O}^+$  into Si @ E = 180 keV

Annealing

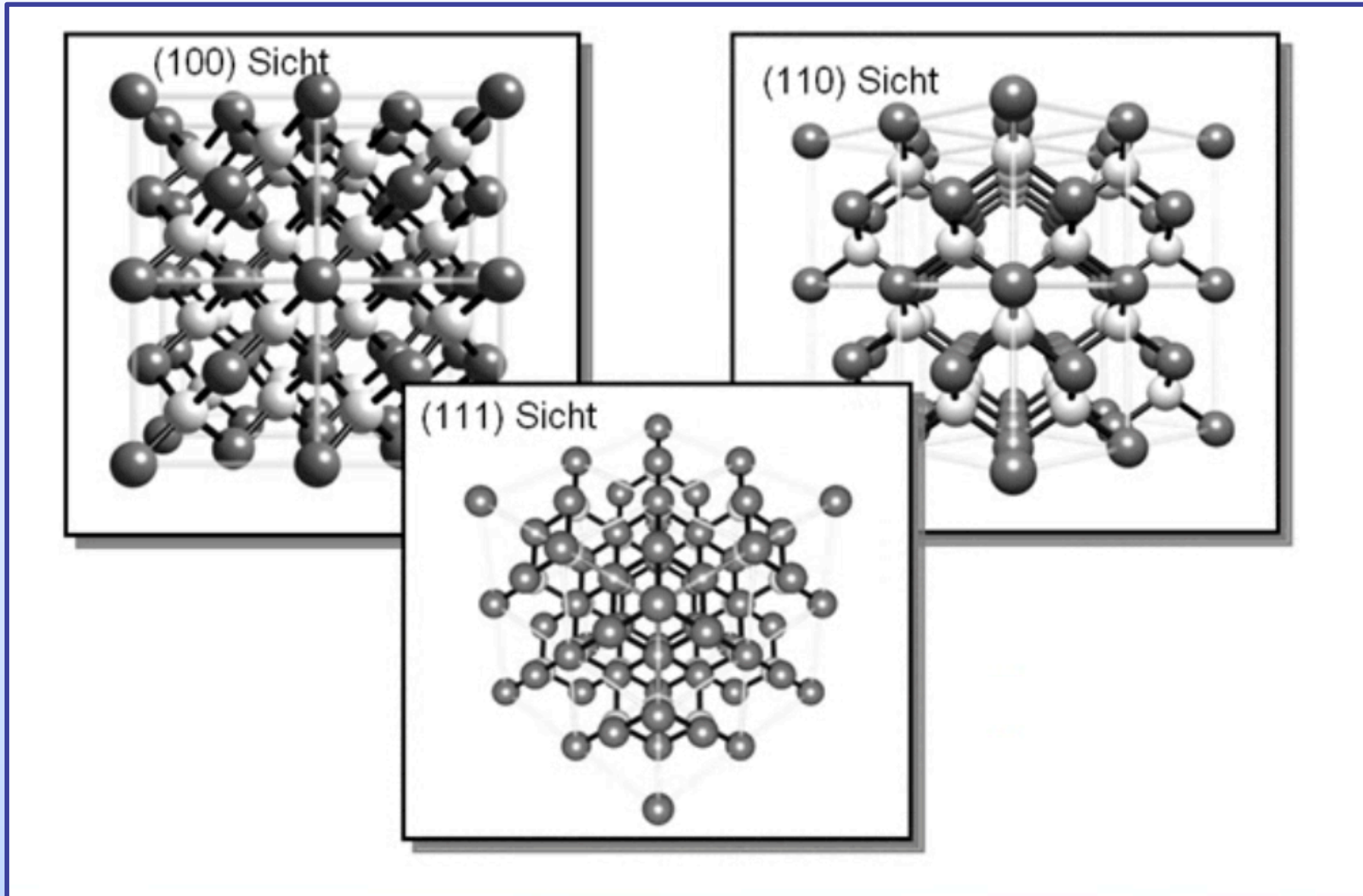
1340 °C in O<sub>2</sub>/Ar atmosphere

O<sub>2</sub>/Ar ration 0.5:100

— R<sub>p</sub>

A. Ogura, H. Onor, Applied Surface Science 159–160 (2000) 104–110

# Channeling



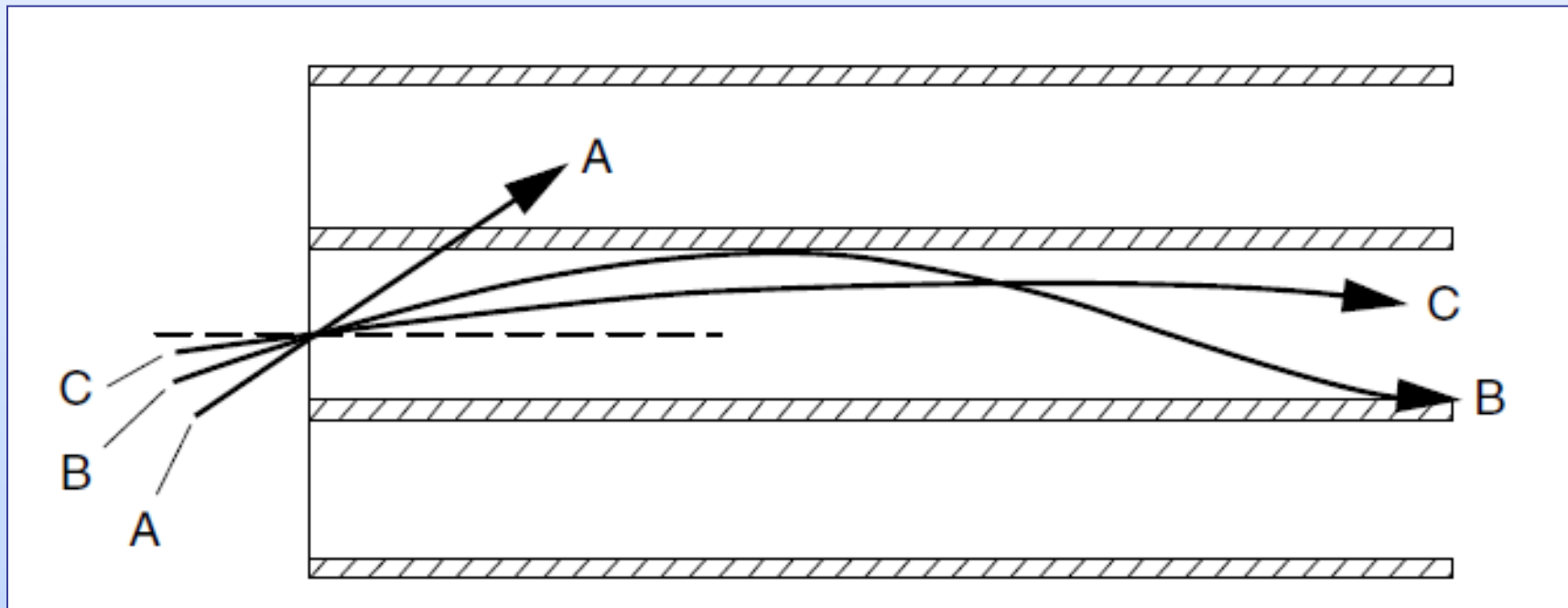


# Channeling

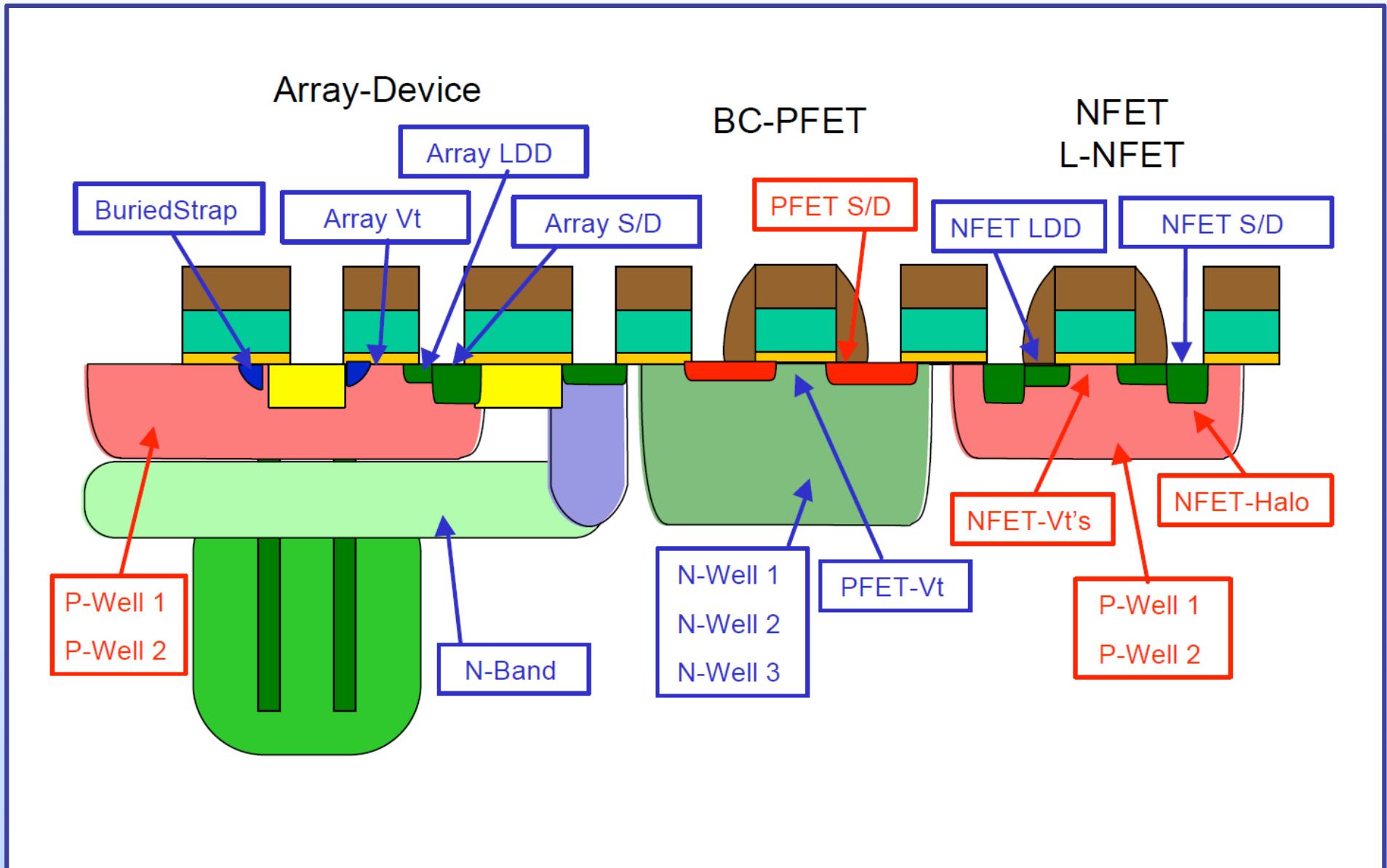
- Entlang bestimmter Kristallrichtungen („Kanäle“) können sich die Ionen mit wesentlich weniger Energieverlust ausbreiten
- Reichweite in solchen „Kanälen“ kann bis zu einer Grössenordnung grösser sein
- Kritischer Winkel liegt zwischen  $3^\circ$  und  $7^\circ$

## Unterbinden des Channeling

- Herausdrehen des Kristalls
- Abscheidung einer amorphen Oberflächenstreichschicht => diffuse Streuung



# DRAM implants steps



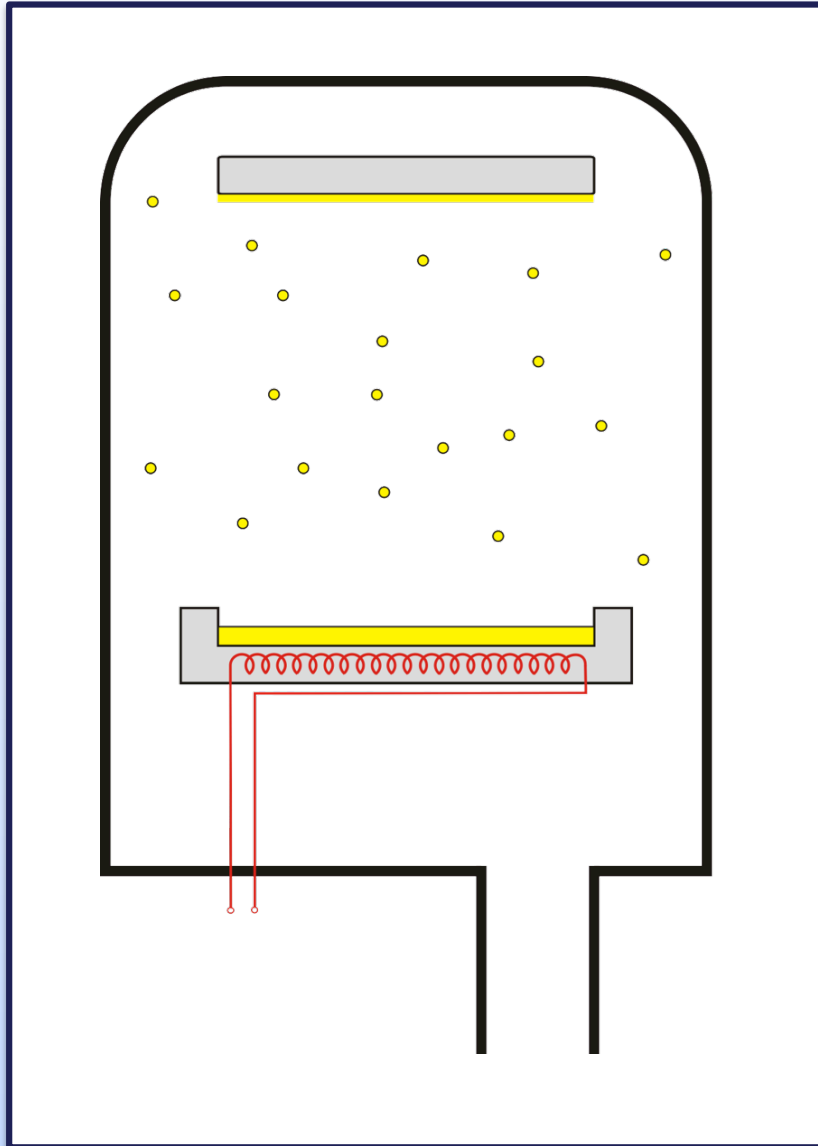
# Ionenbeschleuniger



Uppsala University, The Ångström Laboratory

# Aufdampfen

# Aufdampfen



1. Thermisches Verdampfen von Material
2. Transfer der Dampfteilchen zum Substrat
3. Niederschlag (Kondensation auf kühlem Substrat und Wänden

# Verdampfen

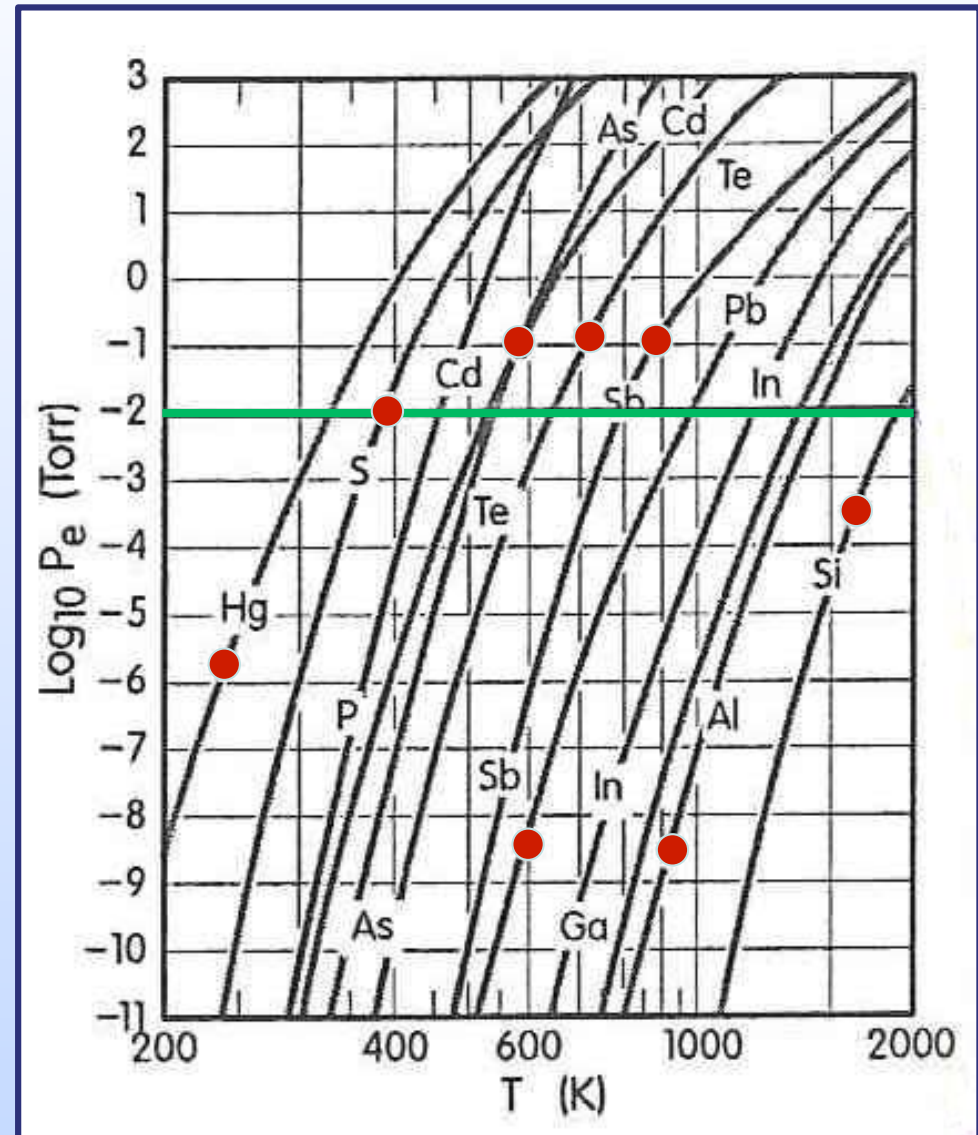
Die Quellematerial wird geheizt um die Dampfdruck zu erhöhen

$$P_e \sim \exp(-B / kT)$$

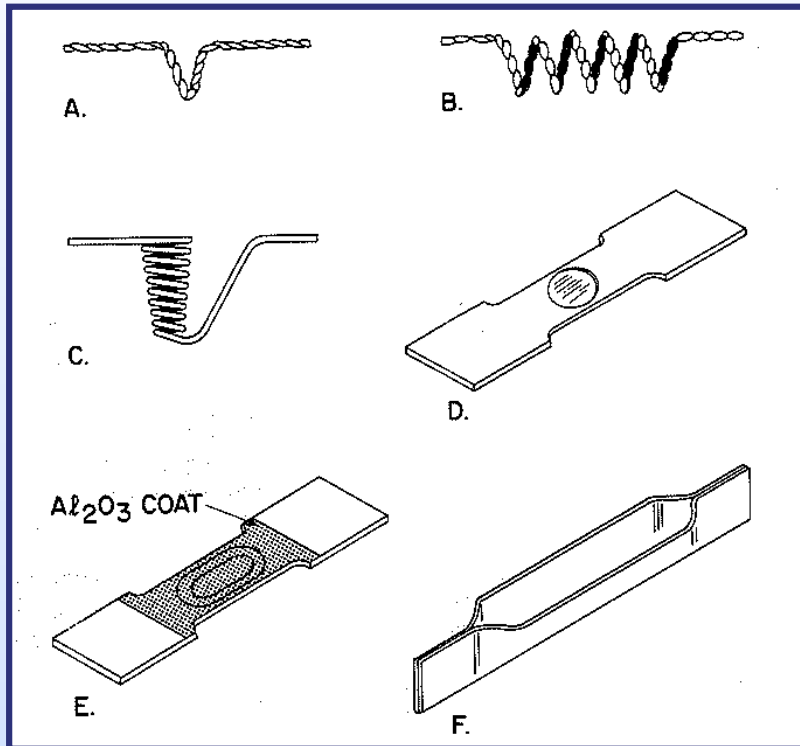
Allgemeiner Regel:  $P_e > 10^{-2}$  Torr

Langmuirsche Gleichung:

$$W = 0.044 \cdot P_e \cdot \sqrt{\frac{M}{T}}$$



# Verdampfungsquellen: Widerstandsheizung



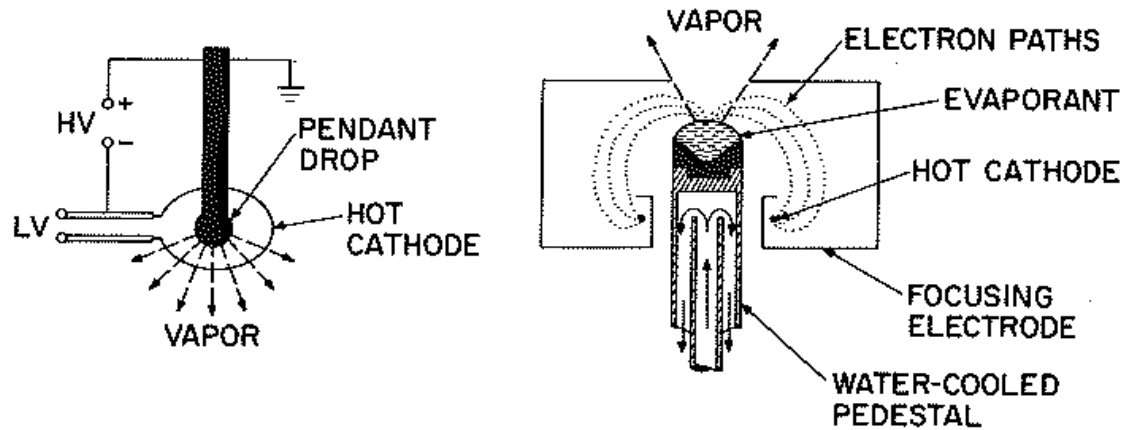
- A Hairpin source
- B Wire helix
- C Wire basket
- D Dimpled foil
- C Dimpled foil with alumina
- F Canoe type

## Materialien:

- Wolfram ( $3380^\circ\text{C}$ )
- Tantale ( $3000^\circ\text{C}$ )
- Molybdän ( $2610^\circ\text{C}$ )

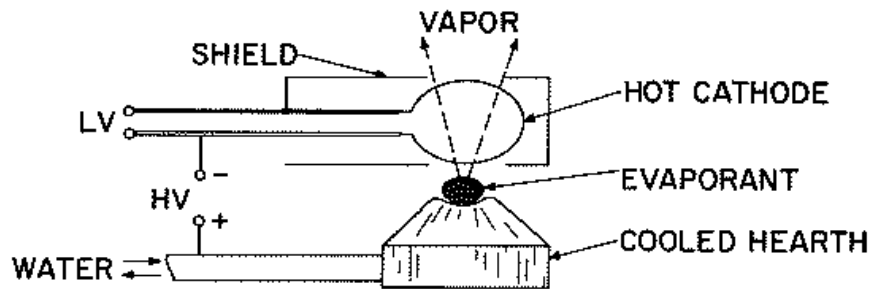
# Verdampfungsquellen: Heizung mit Elektronenstrahl

$E_e = 5 - 10 \text{ keV}$   
 $T \approx 3000^\circ\text{C}$

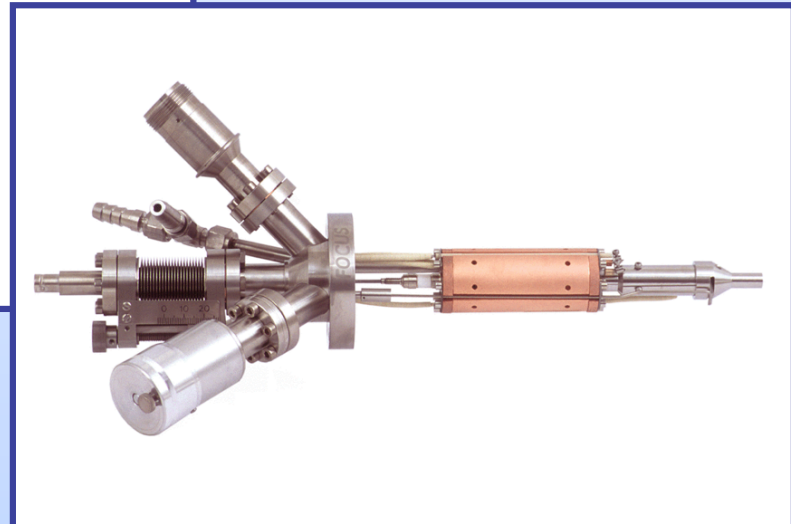


A.

B.

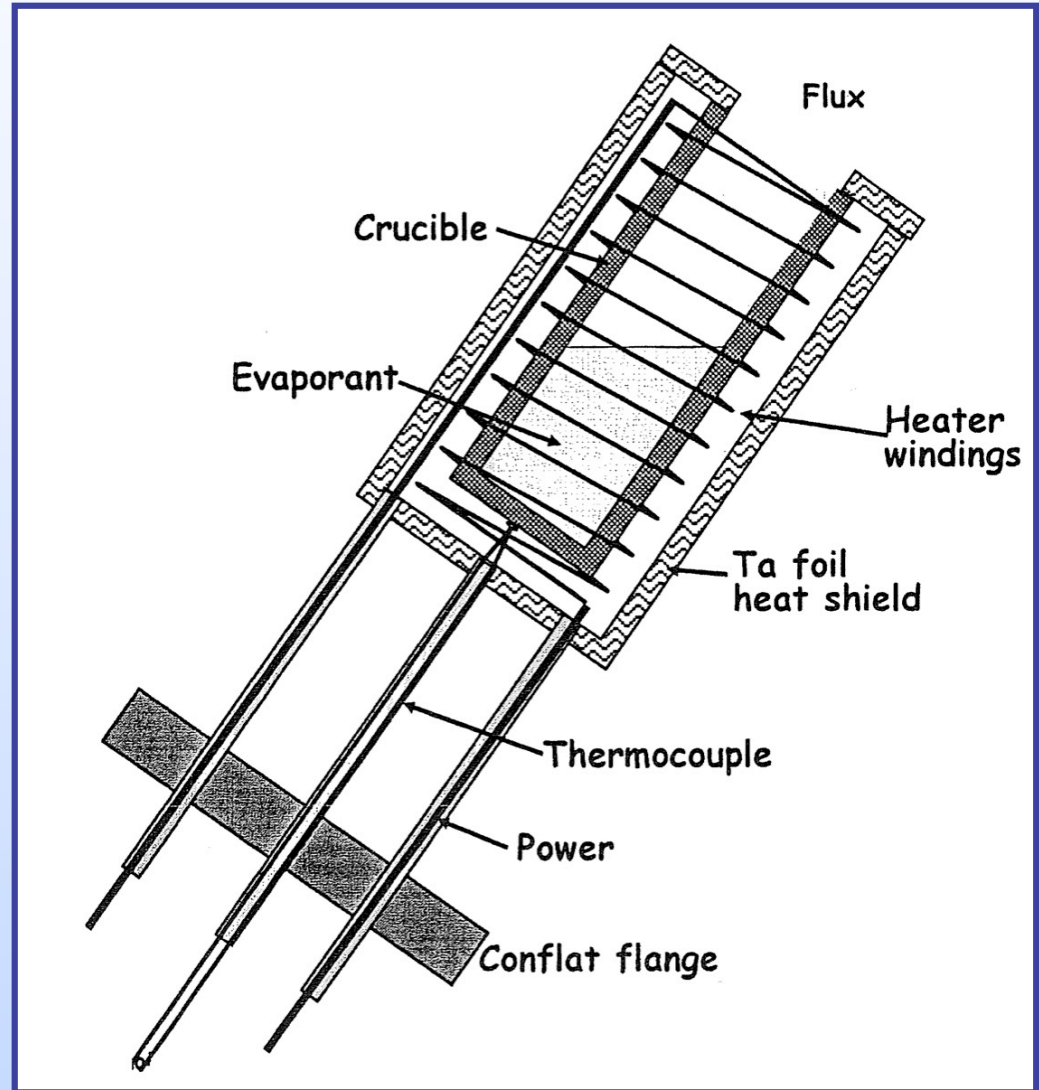


C.

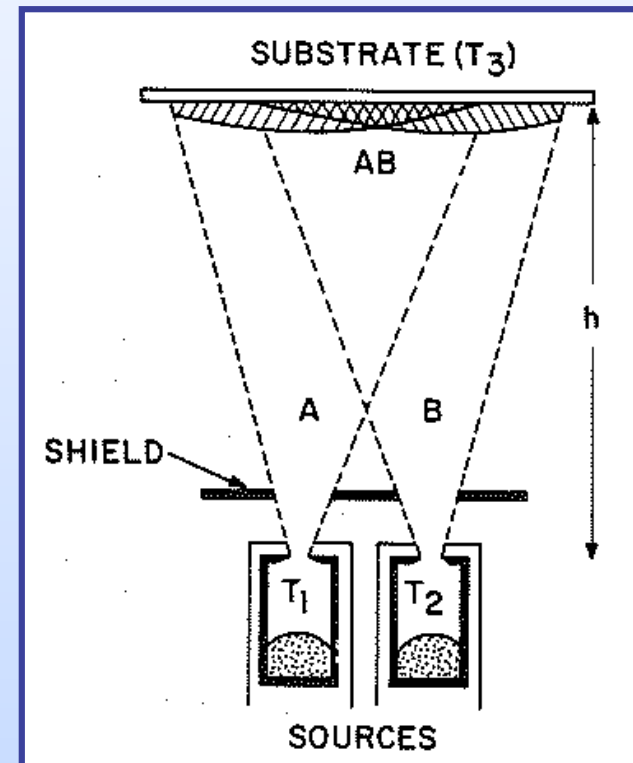
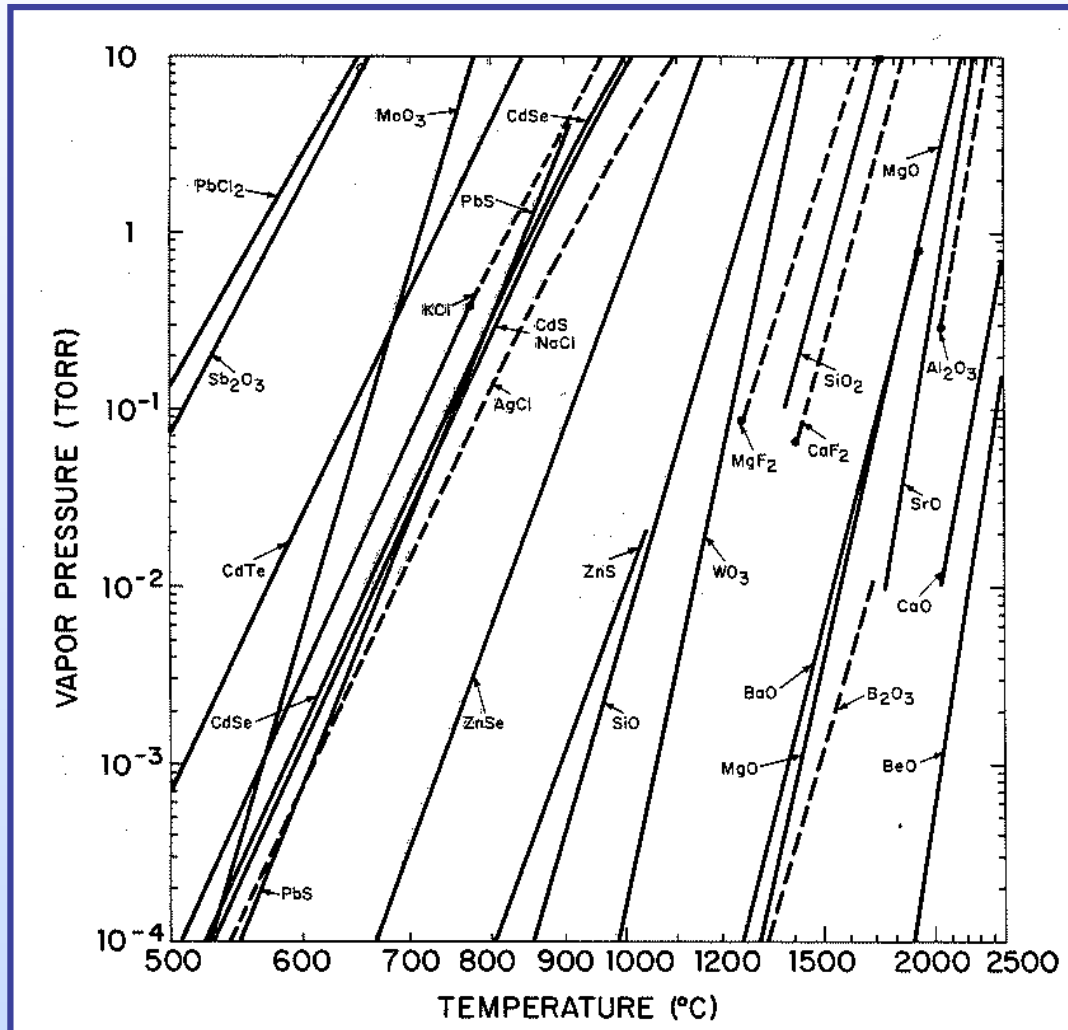




# Effusionszelle (Knudsen Zelle)

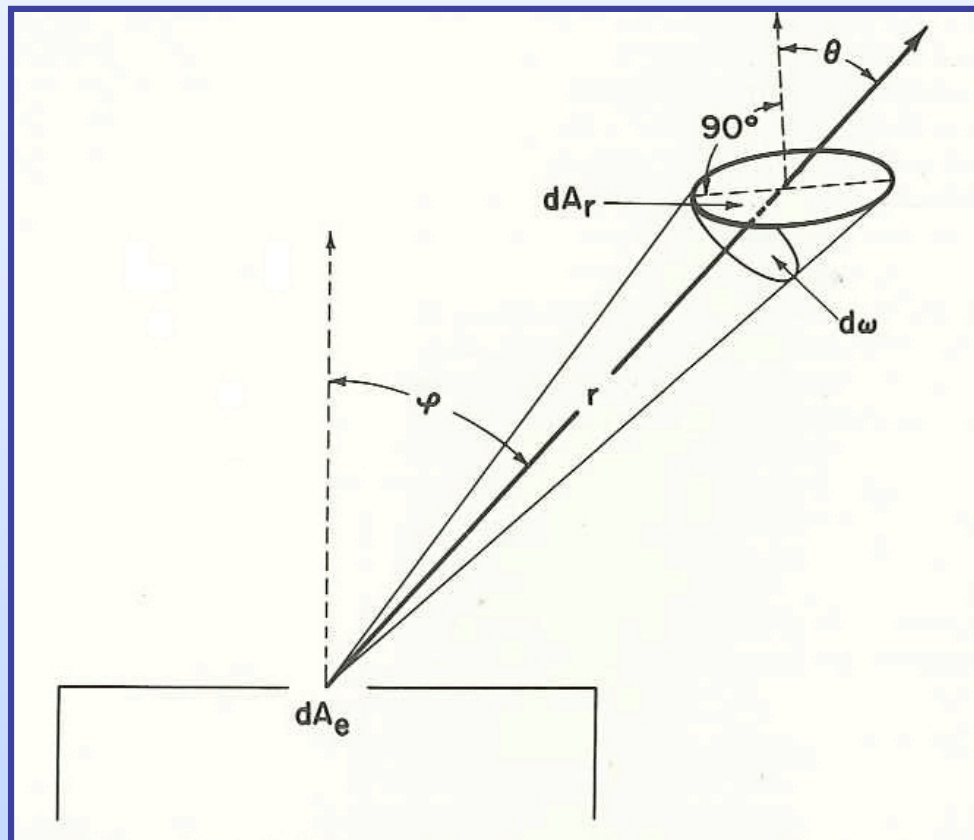


# Aufdampfen von Mischungen



# Verdampfen aus Punktquelle

- Energie der verdampften Teilchen ca. 0.2 eV
- Mittlere freie Weglänge typisch grösser als Dimension des Rezipinten
  - Streuung der Dampfteilchen sind selten

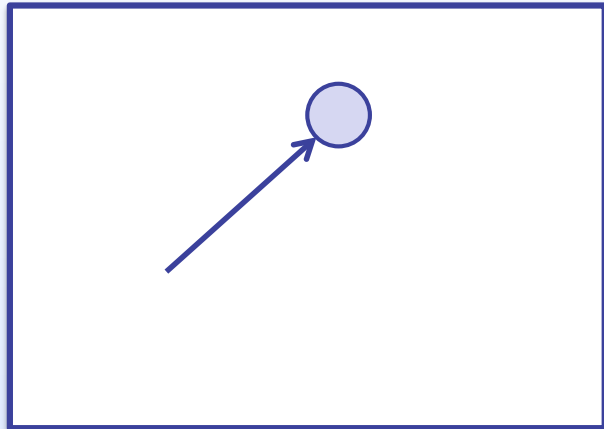


## cos-Gesetz der Emission

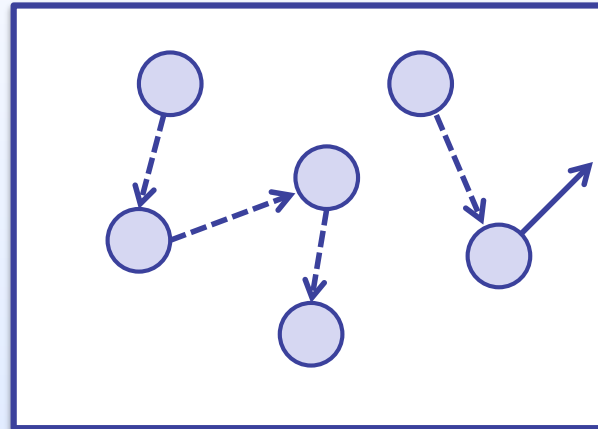
$$\frac{dm}{dt d\omega} = \frac{\Theta_0}{4\pi} \cos \varphi$$

$$d = \frac{1}{\rho} \frac{dm}{dA_r}$$

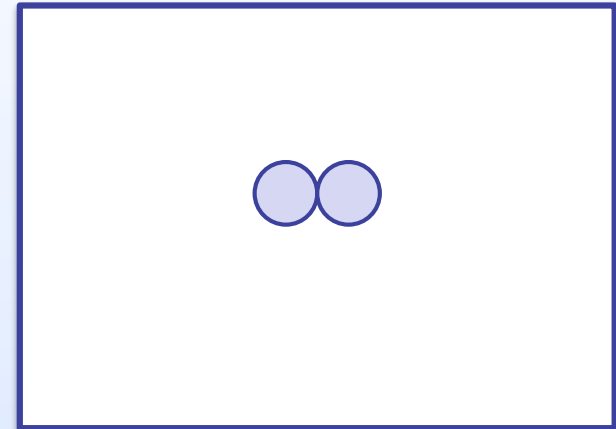
# Growth steps



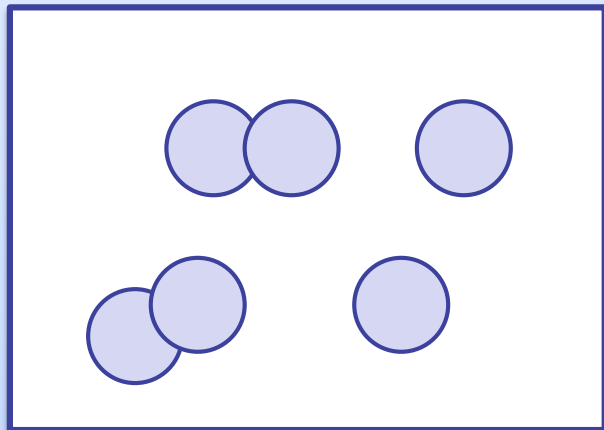
Single atom



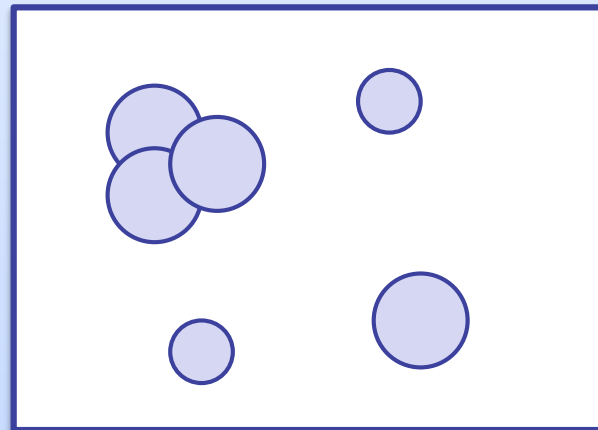
Migration/Re-Evaporation



Collision & Combination of single atoms



Coalescence

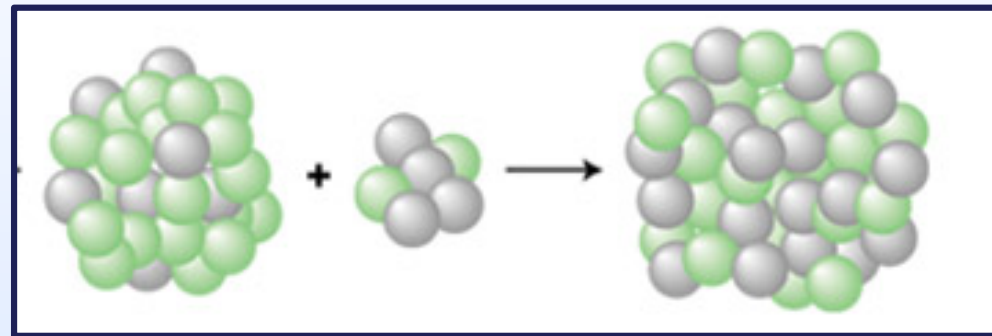


Coarsing (Ostwald ripening)

# Ostwald ripening



Friedrich Wilhelm Ostwald  
1853 – 1932

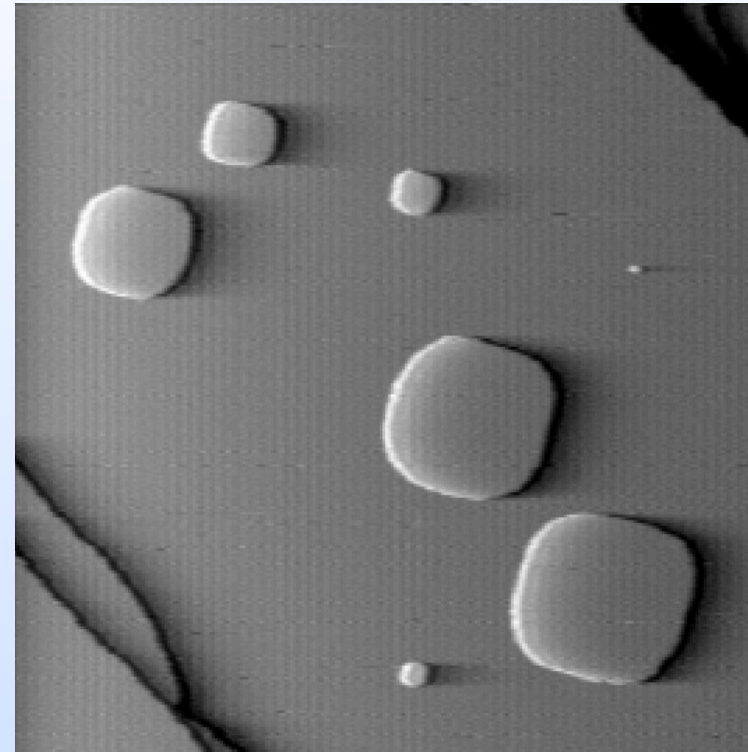
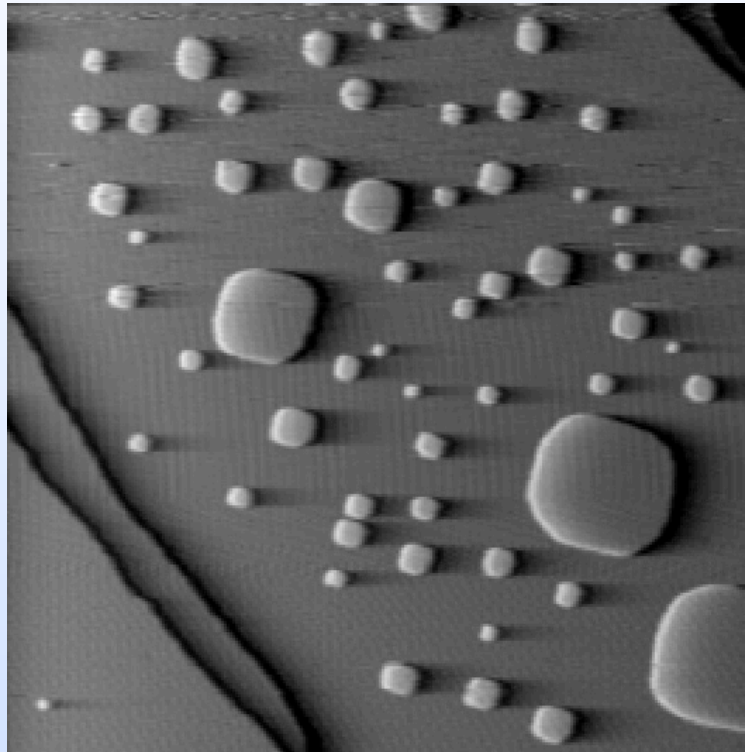


$$\frac{P}{P_e} = \exp\left(\frac{r_{\text{critical}}}{r}\right) = \exp\left(\frac{2\gamma V}{rkT}\right)$$

Gibbs-Thomson Gleichung

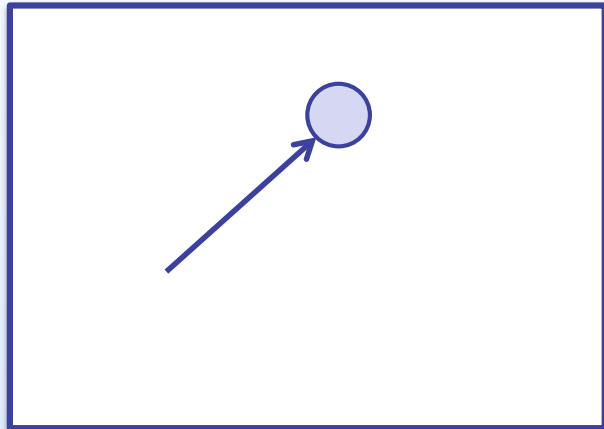
„da nach bekannten Prinzipien ein feines Pulver löslicher sein muss als ein grobes, ebenso wie kleine Tröpfchen einen größeren Dampfdruck haben als große“

# Ostwald ripening

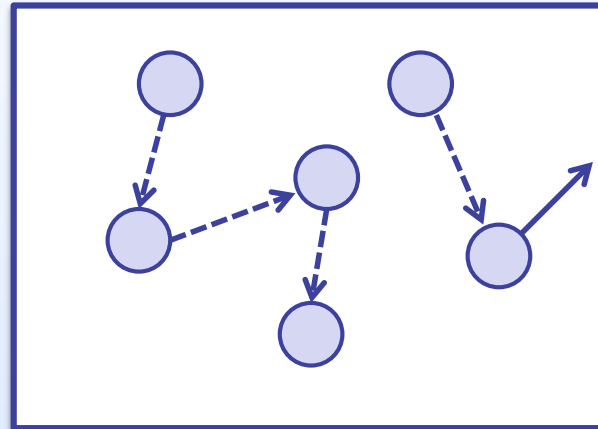


300 nm × 300 nm STM Cu/Cu (001),  $T_s = RT$ ,  $t = 20'000$  sec

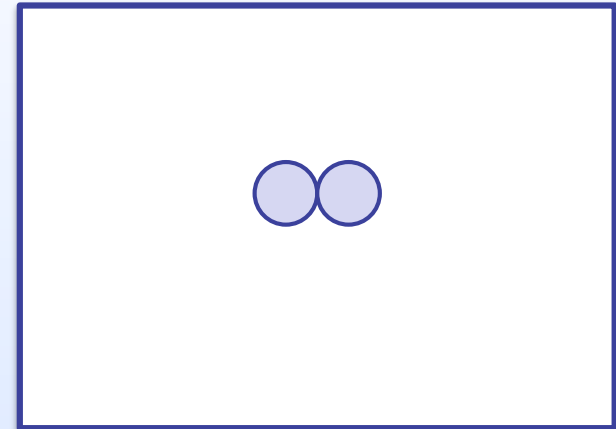
# Growth steps



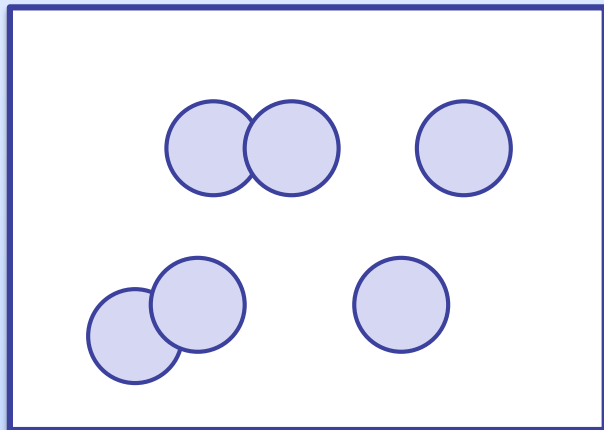
Single atom



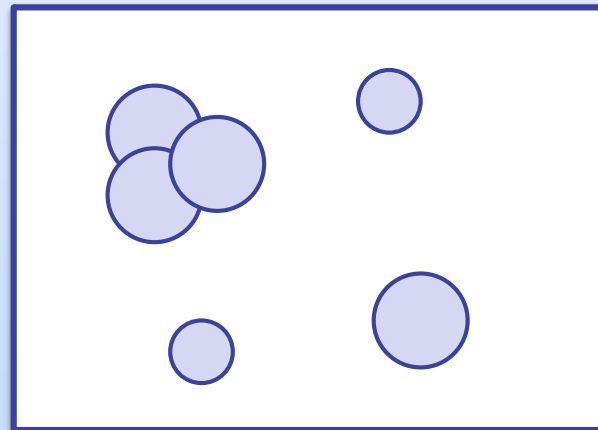
Migration/Re-Evaporation



Collision & Combination of single atoms



Coalescence

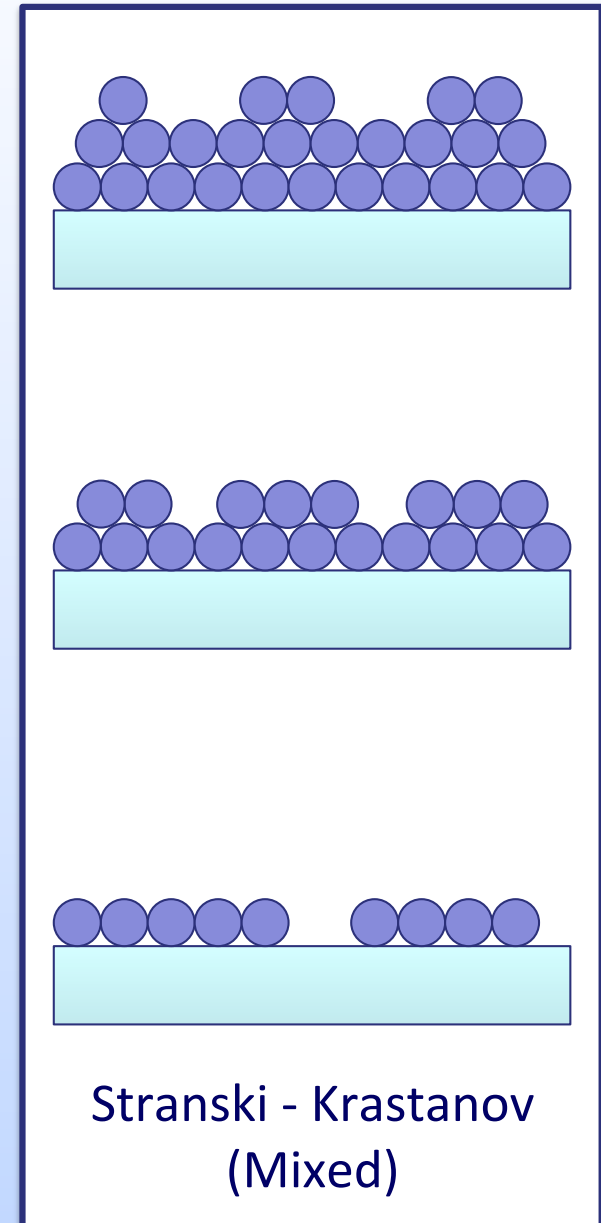
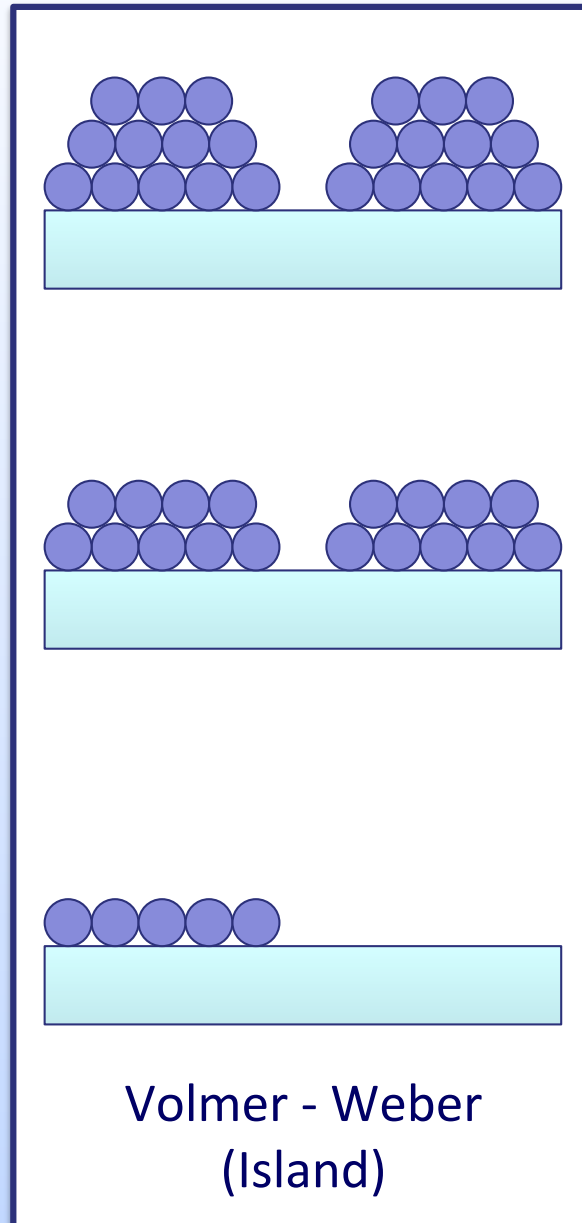
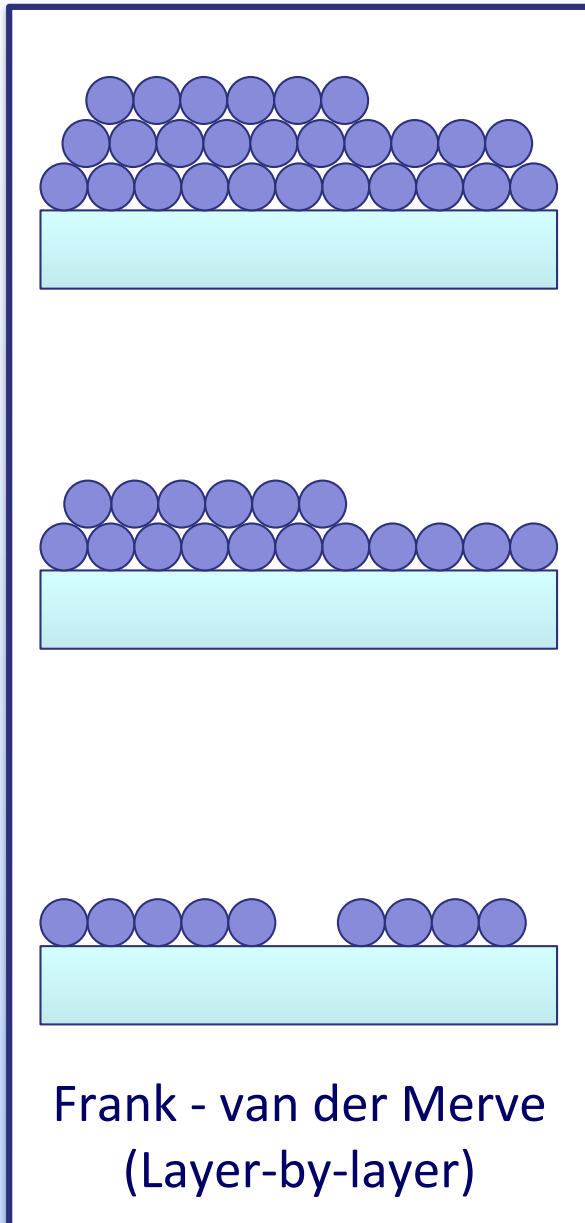


Coarsing (Ostwald ripening)



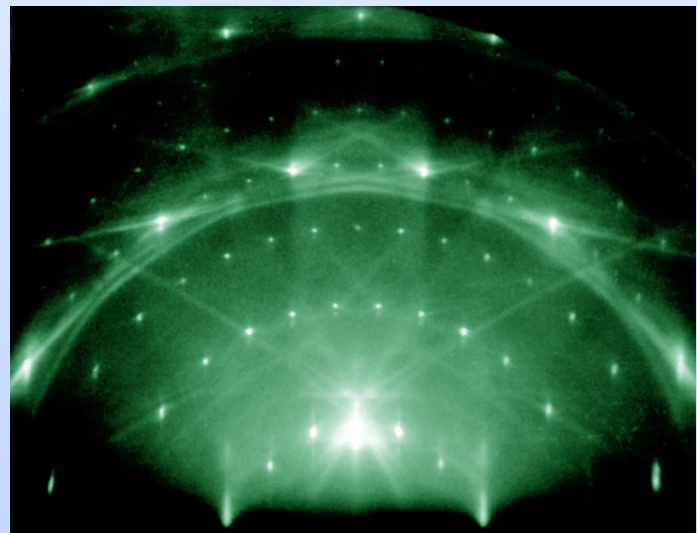
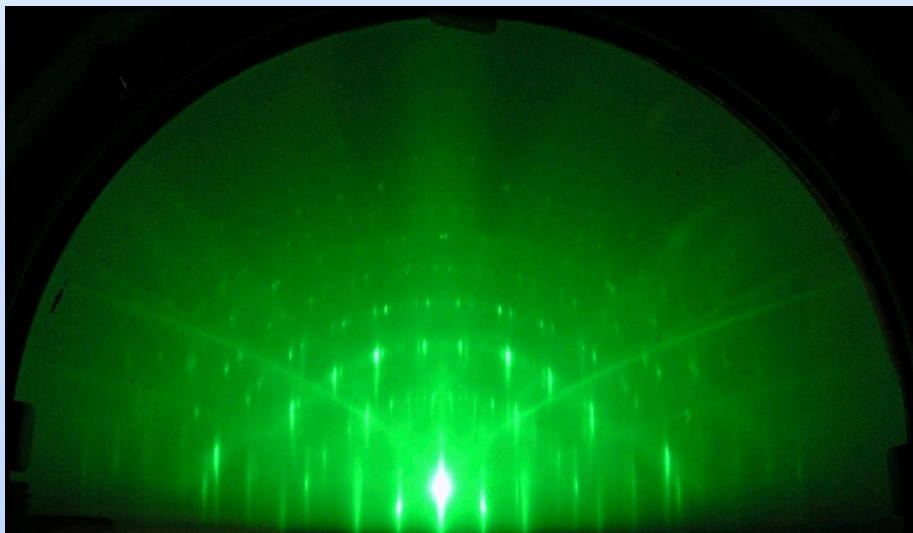
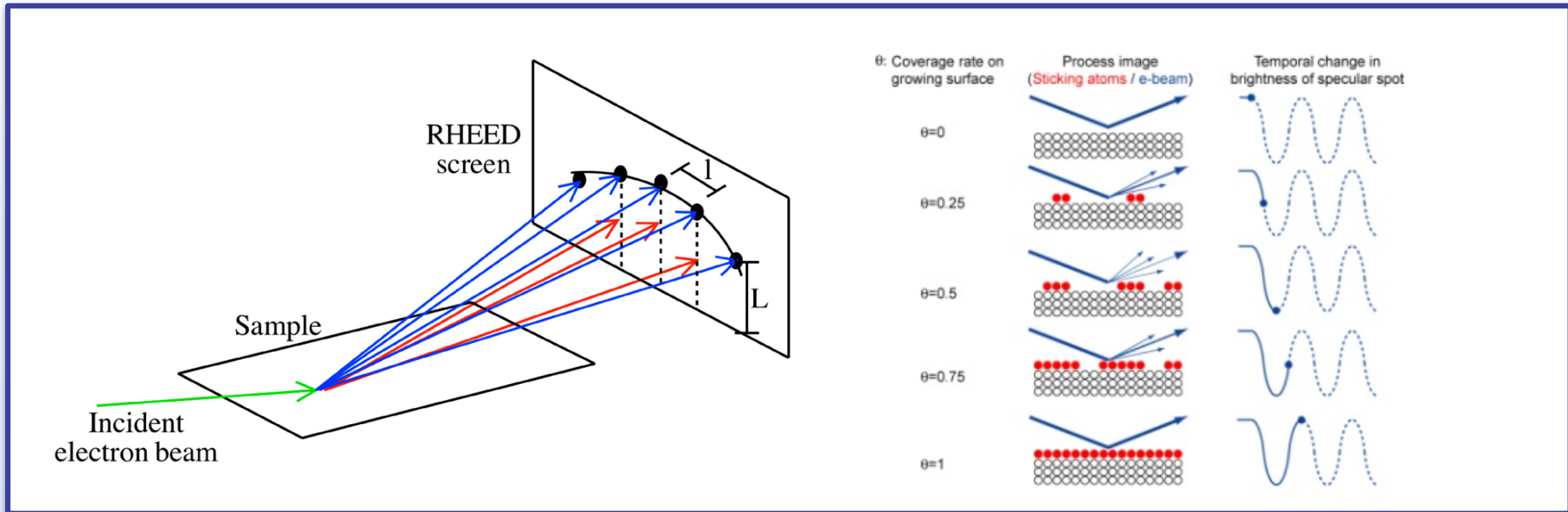
Continuous film

# Growth modes

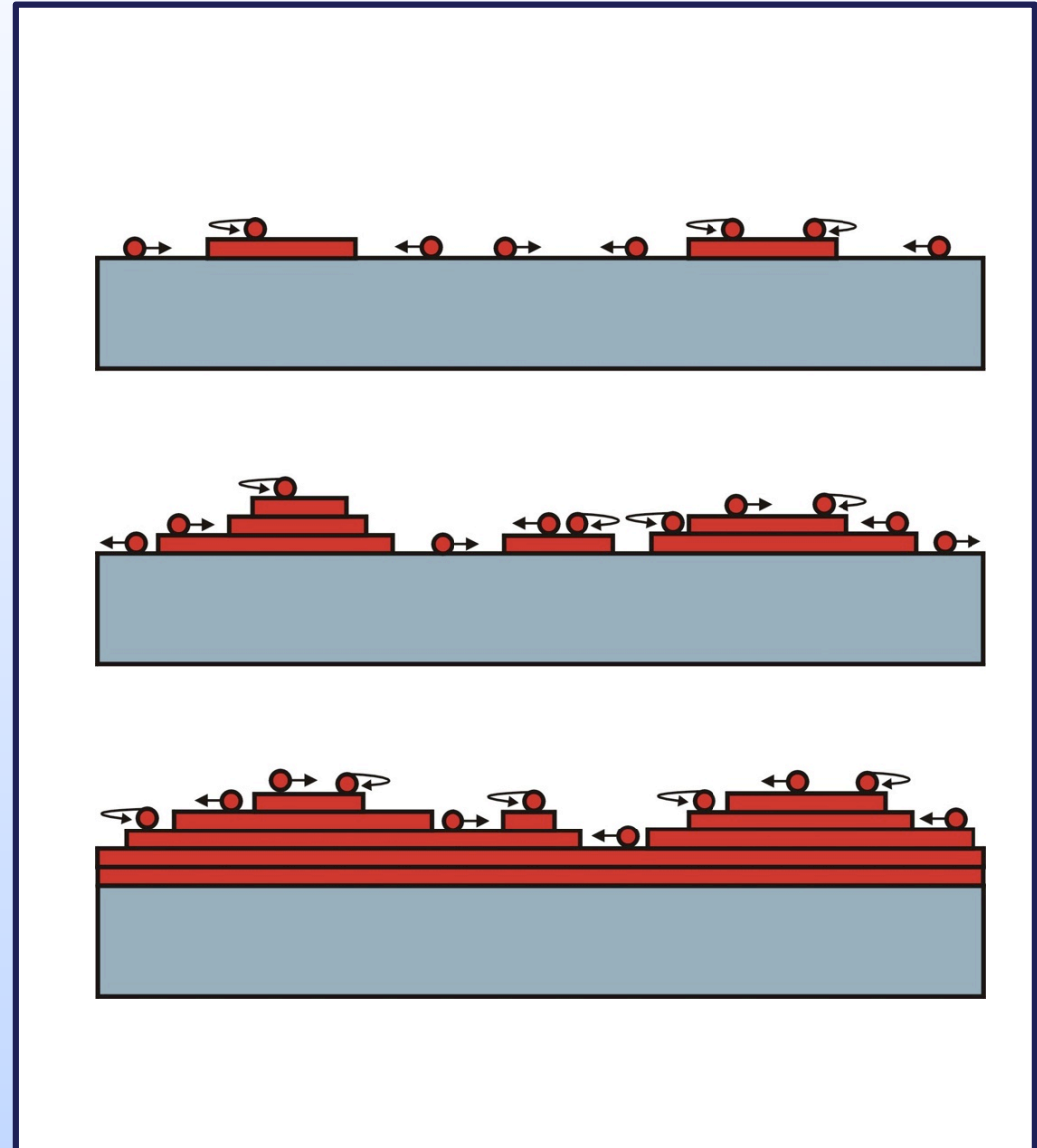
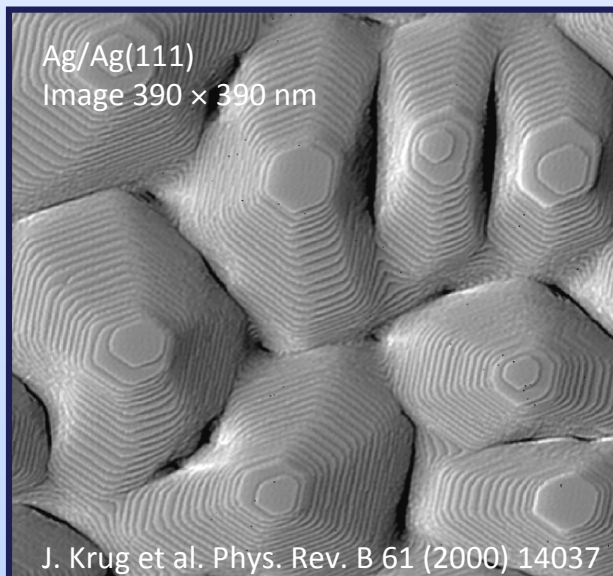
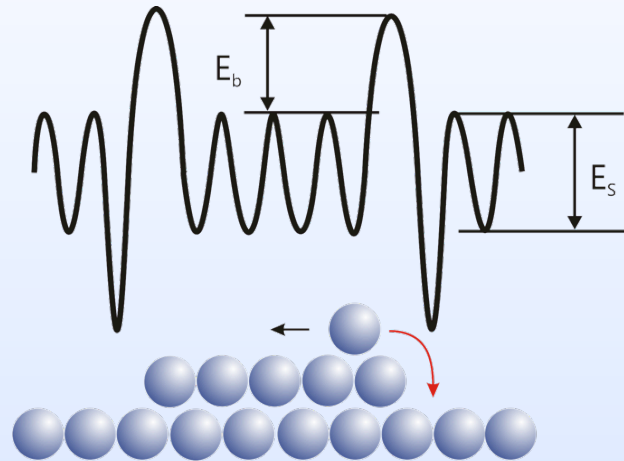




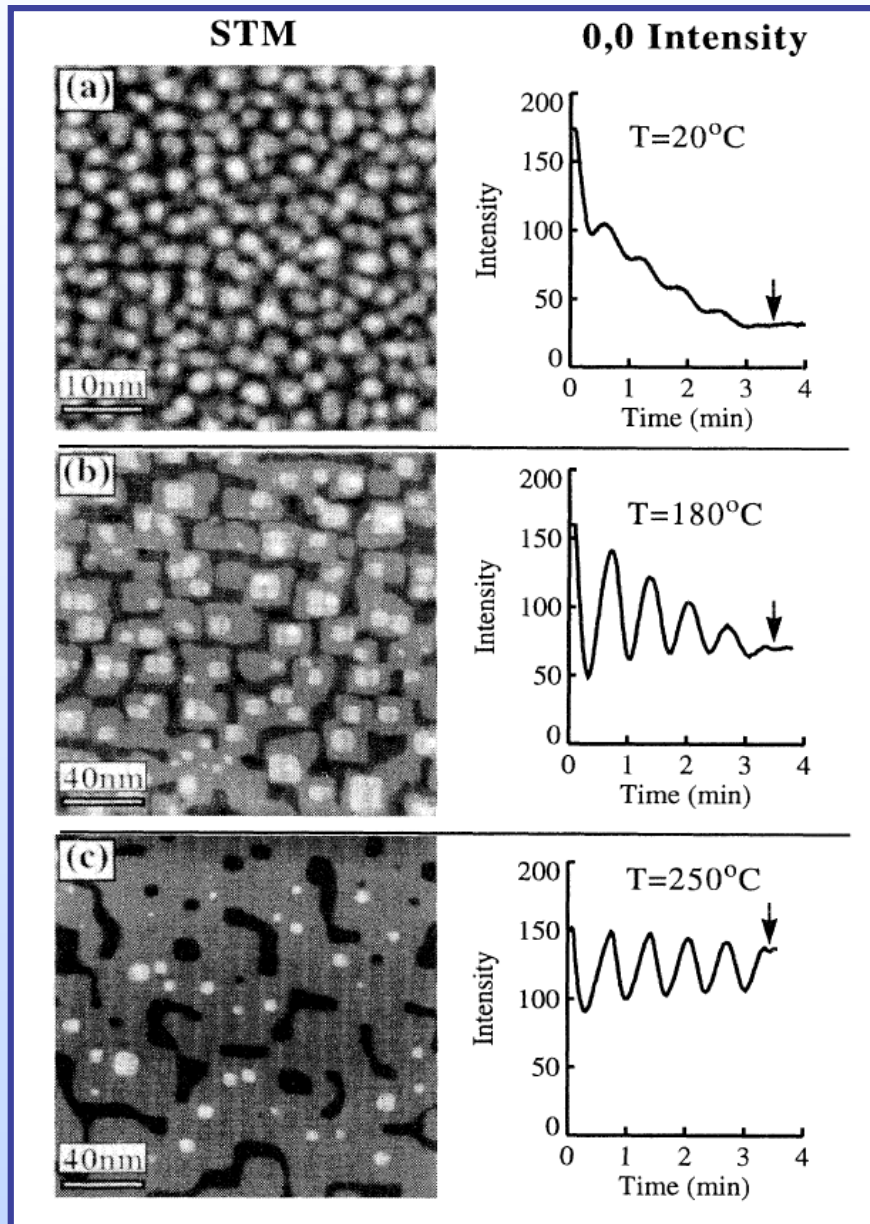
# Reflection High Energy Electron Diffraction



# Ehrlich Barrier



# Homoepitaxy Fe/Fe(100)



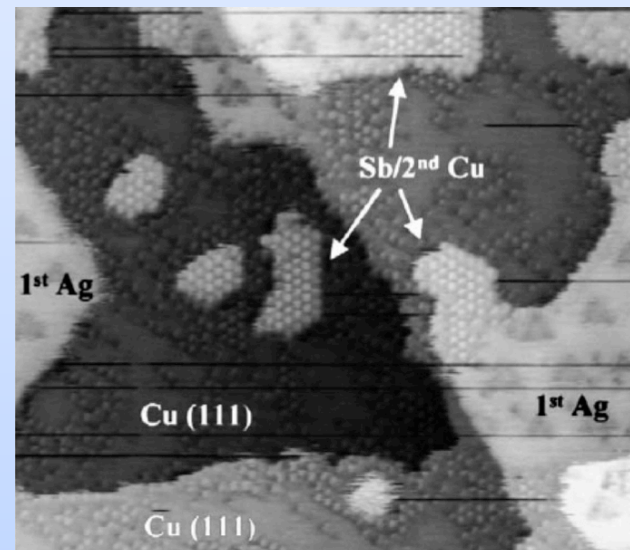
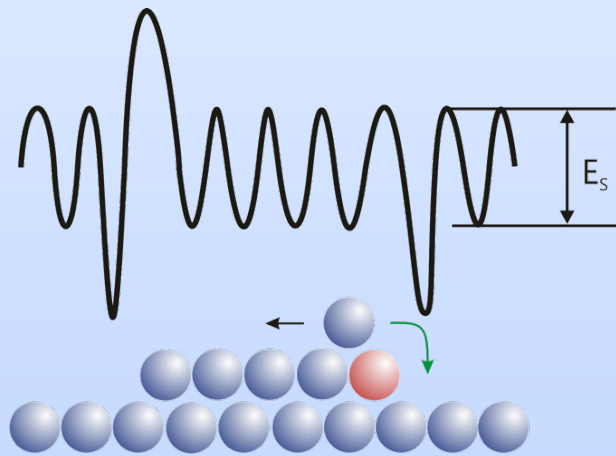
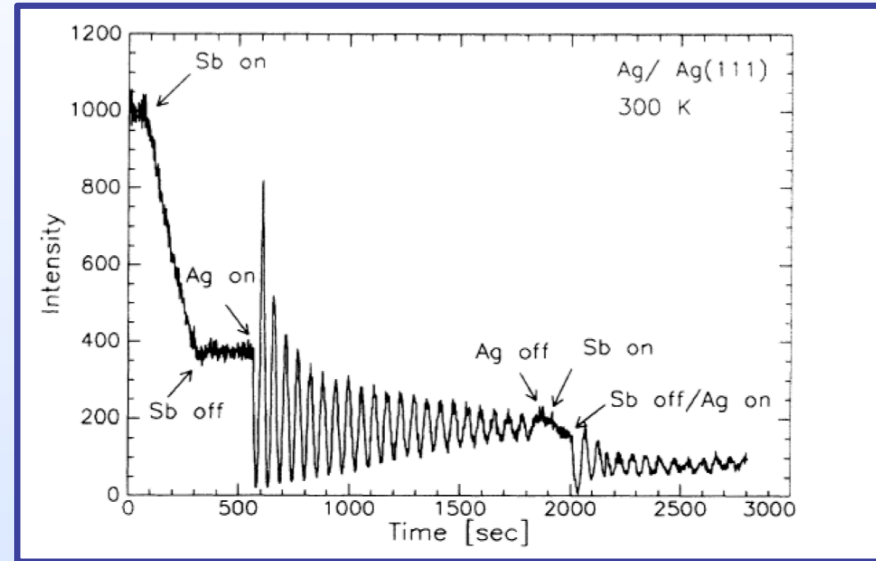
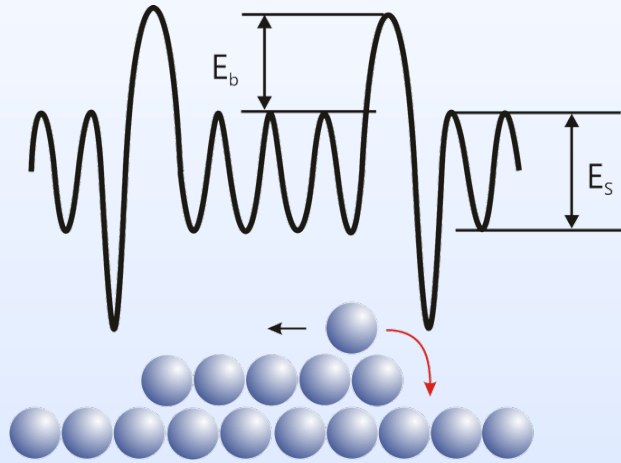
$$\langle s \rangle = 1.74 \text{ nm}^{-1}$$
$$\langle w \rangle = 0.116 \text{ nm}$$

$$\langle s \rangle = 0.23 \text{ nm}^{-1}$$
$$\langle w \rangle = 0.095 \text{ nm}$$

$$\langle s \rangle = 0.09 \text{ nm}^{-1}$$
$$\langle w \rangle = 0.06 \text{ nm}$$

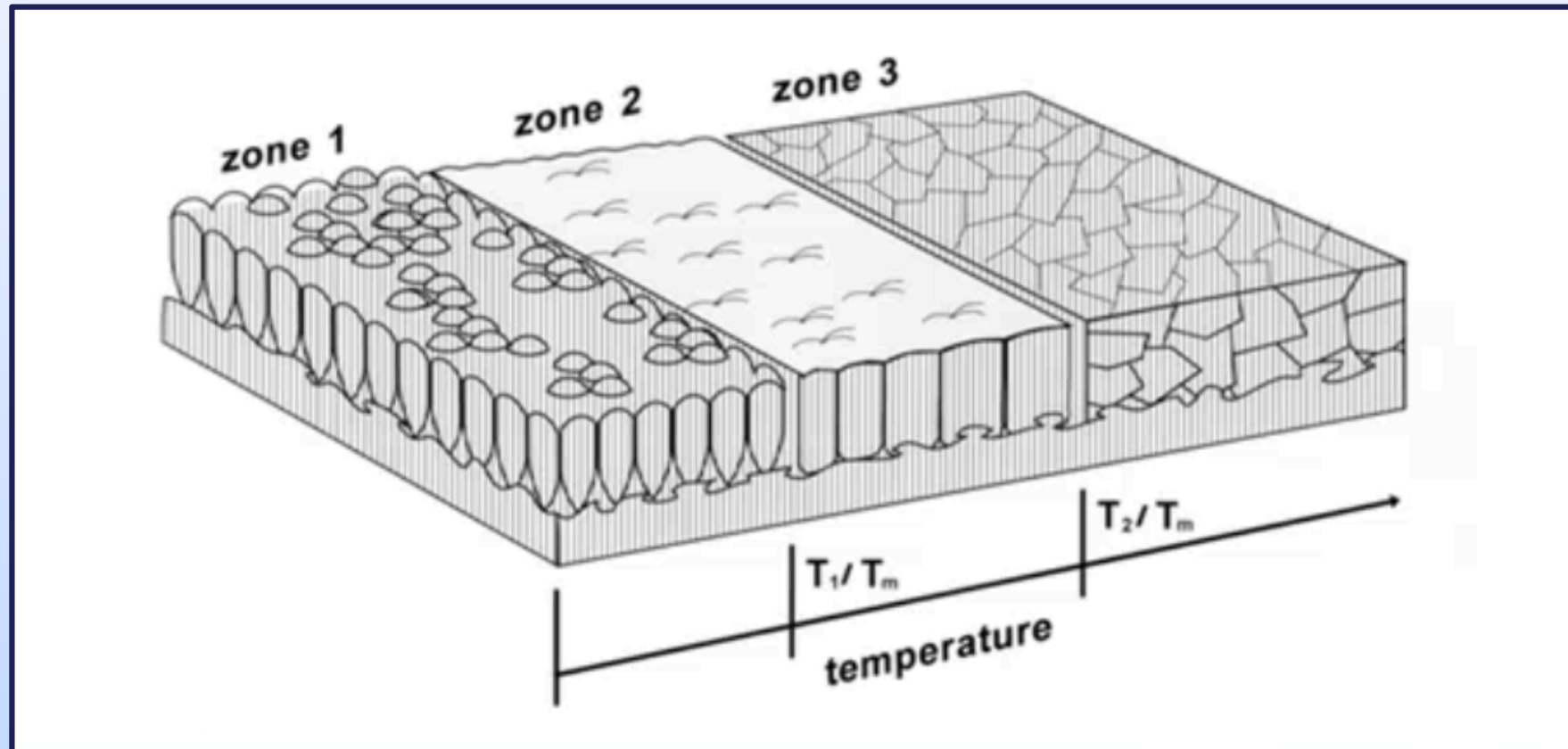
Stroschio et al., Phys. Rev. Lett. 70 (1993) 3615.

# Surfactants



# Morphologie: Movchan und Demchishin Modell

- Dreizonenmodell als Funktion des Temperaturkoeffizienten  $T/T_m$  ( $T_m$  = Schmelztemperatur)
- Untersuchung im Hochvakuum ( $10^{-6}$  –  $10^{-7}$  mbar)



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